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Pilot-scale assessment of the viability of UVA radiation for H_2O_2 or $S_2O_8^{2-2}$

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activation in advanced oxidation processes

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10 Abstract

UVA and UVC radiation were compared for the activation of H_2O_2 or $S_2O_8^{2-}$ to remove 11 12 micropollutants remaining in treated wastewater with a view to optimising the cost and/or the efficiency of the commonly studied UVC/H₂O₂ process. Experiments were carried out in a 13 dynamic laboratory pilot (20 L). In a simple matrix, UVA radiation were able to produce 14 oxydative radicals from H_2O_2 or $S_2O_8^{2-}$, although faster degradation of the estrogens was 15 observed under UVC radiation (up to 55-fold). With both UV radiation, $S_2O_8^{2-}$ was 16 17 photolyzed faster than H₂O₂, resulting in faster estrogen degradation (up to 12-fold). Coupling UVA to H₂O₂ was considered not to be viable because less than 4% of the compounds were 18 degraded at 1000 mJ cm⁻². In a treated wastewater, estrogen degradations were inhibited due 19 to organic matter and stronger inhibitions were observed with $S_2O_8^{2-}$ processes (up to 80%) 20 inhibition compared to simple matrix). The UVC/ $S_2O_8^{2-}$ -process still achieved the fastest 21 degradation rate, but is roughly comparable to the UVC/H₂O₂-process. Very low degradation 22 rates obtained with $UVA/S_2O_8^{2-}$ limit the interest in the process. Experiments were also 23 24 carried out on a mixture of pharmaceuticals leading to similar conclusions.

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26 Keywords: AOPs, micropollutants, photolysis, pilot scale, UVA radiation, wastewater.

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1. Introduction

29 Water scarcity is about to be one of the major challenges of the next decades. The European 30 Union Water Framework Directive adopted in 2000 aims at protecting the quality and the 31 quantity of water bodies in the European Union. Although significant improvements were 32 observed within the last decades regarding the quality of water bodies, the presence of 33 anthropogenic micropollutants in surface and ground waters is increasingly reported. 34 Wastewater treatment plants (WWTPs), whether they are conventional or wetlands, are one of 35 the major gateways of micropollutants to the environment because a large panel of 36 compounds is refractory to the treatments that are commonly used. As a consequence, 37 effluents are released to the environment with micropollutants at concentrations up to several tens of $\mu g L^{-1}$ [1, 2, 3]. Improving the removal of micropollutants in WWTPs by the use of 38 39 appropriate treatments would allow the discharge of water of better quality. Moreover, it 40 could promote effluent reuse for crop fields irrigation or industrial use for example and 41 decrease the pressure on aquatic environments.

42 In France, more than 90% of the WWTPs are small and medium-sized (< 10,000 population 43 equivalent) and around 40% are equipped by nature-based processes such as constructed 44 wetlands (CWs) [4]. These plants have different human and technical resources and therefore 45 different needs compared to large-scale urban WWTPs. They require cheap, reliable and low-46 maintenance processes. Among the existing treatments for micropollutants, photoactivated 47 advanced oxidation processes (AOPs) seem to meet these criteria. They consist in the generation of highly oxidising species such as HO $(E_{HO}^0/_{HO}^- = 2.80 \text{ V/SHE} \text{ at } 25 \text{ °C})$ by the 48 49 photolysis of an oxidant precursor (typically H₂O₂). The abilities of the UVC/H₂O₂ process

have been widely reported. Cédat et al. [5] observed the complete degradation of a mixture of three estrogens (5 μM each spiked in a WWTP effluent) and of their estrogenic activity and estimated the cost of the technology to be under $0.20 \in m^{-3}$. However, UVC radiation is generally produced by mercury lamps which are quite energy consuming. In the UVC/H₂O₂ process, Cédat et al. [5] estimated that electricity would represent from 14 to 38% of the total treatment cost. Moreover, H₂O₂ supply is another significant expenditure item since it was estimated to represent from 47 to 62% of the total cost.

57 With a view to optimising the efficiency/cost ratio of the AOP, alternatives to the UVC/H₂O₂ 58 treatment were presented in the literature. For example, the abilities of $S_2O_8^{2-}$ as an oxidant 59 precursor to generate two sulfate radicals (SO₄⁻) ($E_{SO_4^-/SO_4^{2-}}^0 = 2.5 - 3.1$ V/SHE at 25 °C,

60 depending on the solution pH) by photolysis have been widely shown [6, 7, 8].

61 Then, another alternative is the use of solar light as a UV source. Incident solar radiation on 62 earth is a free and renewable energy, composed of 95% of UVA and 5% of UVB and it was previously reported in the literature that UVA radiation is able to photolyse H_2O_2 and $S_2O_8^{2-1}$ 63 [9, 10]. Fernandes et al. [11] also recently demonstrated that natural solar radiation is efficient 64 65 in activating these oxidant precursors. Kowalska et al. [12] and Moreira et al. [10] observed complete degradation of carbamazepine and diclofenac in spiked effluents under solar 66 67 radiation coupled to H₂O₂. Finally, Rizzo et al. [13] and Velo-Gala et al. [14] both compared the efficiency of a solar simulator to UVC radiation for the activation of H₂O₂ in order to 68 69 degrade antibiotics in small volumes (0.5 and 6 L respectively). In both studies, the lower 70 efficiency of solar light compared to UVC radiation was concluded. However, the reported 71 degradation rates were time-dependent and no comparison of the energy required (UV 72 fluence) in each process was made.

Since UVA radiation constitute the majority of solar UV, it seems essential to evaluate their
abilities for the activation of oxidant precursors in AOPs. To the best of our knowledge, no

75 previous study has compared UVA to UVC radiation for the photo-activation of H_2O_2 and 76 $S_2O_8^{2-}$.

In the present work, an intermediate-scale laboratory pilot (maximum capacity of 50 L) was 77 used to compare UVA to UVC radiation for the activation of H_2O_2 or $S_2O_8^{2-}$. H_2O_2 was 78 79 chosen for its ease of implementation and the large number of studies identified in the literature. $S_2O_8^{2-}$ was studied for its high efficiency with the aim of assessing whether its use 80 81 could balance the expected loss of efficiency when replacing UVC by UVA radiation. For 82 technical reasons, mercury lamps were used for the production of both types of radiation, 83 allowing UV fluence calculation and comparison. Three estrogens, namely estrone (E1), 17β-estradiol (E2) and 17α-ethinylestradiol (EE2), were first chosen as model pollutants for 84 85 process efficiency assessment. According to Ilyas and van Hullebusch [15], they are removed from 30 to 80% in constructed wetlands, due to biodegradation, plant uptake and adsorption, 86 leading to concentrations from ng L^{-1} to several $\mu g L^{-1}$ in the released effluent. Similar 87 88 degradation rates are also achieved in conventional WWTPs [16, 17]. Nevertheless, their 89 occurrence in surface waters and river sediments as well as their ecotoxicity at environmental 90 concentrations have been widely reported [18]. Finally, a mixture of ibuprofen, (IBU), 91 naproxen (NAP) and diclofenac (DCF), three commonly detected non-steroidal anti-92 inflammatory drugs, allowed to confirm the results on another type of micropollutants.

93

2. Materials and methods

94 2.1. Chemicals and reagents

Estrone (E1), 17β-estradiol (E2), 17α-ethinylestradiol (EE2), ibuprofen (IBU) sodium salt, diclofenac (DCF) sodium salt and naproxen (NAP) were purchased from Sigma-Aldrich, as well as H_2O_2 (30% in water) and $Na_2S_2O_8$. Persulfate stock solutions were prepared in drinking water (1 M). E1, E2, EE2 and NAP stock solutions were prepared at 5 mM in acetonitrile. IBU and DCF stock solutions were made at 10 mM in drinking water. Acetonitrile (ACN) was supplied by VWR Chemicals (HPLC grade). Ultrapure water was
obtained from a milli-Q system. Formic acid was purchased from Chimie-plus Laboratoires.

- 102 2.2. Irradiation experiments
- 103 2.2.1. Description of the laboratory pilot

104 The experimental set-up has previously been described in the literature (Cédat et al., 2016) 105 and is reproduced Figure 1. It is composed of a 50-L glass tank linked to a 1.12-L UV reactor (COMAP) by a centrifugal pump. In the reactor, the UV lamp is protected by a quartz tube 106 107 and the effluent flows through a 1-cm layer around the tube. Effluent recirculation allows to 108 increase the contact time between the targets and the lamp and thus the UV fluence. Low pressure mercury lamps (Philips) were used for the generation of UVC and UVA radiation. 109 110 The UVC lamp was monochromatic while the UVA lamp was polychromatic and emits from 111 345 to 410 nm with a maximum at 365 nm (Figure SM1). Their technical features are 112 presented in Table 1.



- 114Figure 1. Schematic diagram of the pilot used, reproduced from Cédat *et al.*, 2016. 1) Glass tank; 2) pump; 3)115flow meter; 4) and 6) sampling points; 5) UV reactor; 7) UV intensity control; 8) temperature control.
- 116



Table 1. Technical characteristics of UVA and UVC lamps.

UV type	Lamp power (W)	Power efficiency	Wavelength (nm)	Length (cm)	Hg (mg)
UVC	54	32%	254	60.0	8.0
UVA	36	24%	345 - 410	89.5	2.0

The UVCalc®2A software (Bolton Photosciences Inc., Canada) was used for UV fluence calculations. On the advice of the software designer and given its narrow emission spectra, the UVA lamp was considered monochromatic. After calculation, a correction factor of 0.88 for UVC radiation [5] and 0.82 for UVA radiation (software designer recommendations) was applied.

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2.2.2. Matrix composition

Main physico-chemical parameters of the matrices used to investigate the degradation of micropollutants are presented in Table 2. Drinking water collected directly to tap (Villeurbanne, France) was first used as a simple matrix. Then, WWTP effluents were collected in 30-L plastic containers at the outlet of a conventional WWTP equipped by an activated sludge treatment (Feyssine, Villeurbanne, France) with a capacity of 300,000 population equivalent. Samples were collected in the morning and used within 30 hours.

130

Table 2. Main physico-chemical parameters of drinking water and WWTP effluents.

	Drinking water	WWTP	WWTP
	Diffiking water	effluent 1	effluent 2
pH	7.7	7.8	7.9
UV _{254nm} transmittance	98%	62%	61%
UV _{365nm} transmittance	> 99%	90%	87%
Conductivity (μ S cm ⁻¹)	395	913	912
Suspended solids (mg L^{-1})	-	4	4
Chemical Oxygen Demand (COD) (mg L ⁻¹)	< 5	29	26
Total Organic Carbon (TOC) $(mg_C L^{-1})$	-	7.5	5.8
$\operatorname{Cl}^{-}(\operatorname{mg} \operatorname{L}^{-1})$	10	107	98
NO_{3}^{-} (mg L ⁻¹)	5.1	21.2	24.6
$HCO_3^{-} (mg L^{-1})$	220	208	252

131 2.2.3. Experimental procedures

The laboratory pilot was used to determine the photolysis constants of the oxidant precursors, the photolysis first order rate constants of the estrogens and the overall pseudo-first order degradation rate constant of the estrogens or of the pharmaceuticals obtained through the experiments. Experimental procedures were quite similar and operating conditions are

136 summarized in Table 3. The experimental set-up was filled in to 20 ± 0.5 L with the matrix. Then, recirculation flow was set at 20 ± 0.5 L min⁻¹, the UV lamp was pre-heated during 137 10 minutes and the temperature was adjusted and stabilised at 22 ± 2 °C. After pre-heating, 138 the lamp was turned off and the solution was spiked with 3 estrogens or 3 pharmaceuticals at 139 140 5 µM each (except for the experiments regarding oxidant precursor photolysis). Although this 141 concentration is higher than those in WWTP effluents, it does not require pre-concentration 142 prior to ultra high-performance liquid chromatography (UHPLC) analysis and therefore 143 allows the sampling of small volumes, suitable for kinetic experiments. Then, an appropriate volume of oxidant precursor was added: 10.3 mL of H_2O_2 (30%) or 100 mL of a 1 M $S_2O_8^{2-1}$ 144 145 stock solution were added to reach a concentration of 5 mM ; 2.06 mL of H₂O₂ (30%) and 20 mL of $S_2O_8^{2-1}$ M were added to reach a concentration of 1 mM. No oxidant precursor was 146 147 added for estrogen photolysis experiments. For oxidant precursor photolysis only, 100 mL of 148 methanol (0.5% v/v) were also added: methanol quenches the newly formed hydroxyl or sulfate radicals to prevent them from reacting in turn with H_2O_2 or $S_2O_8^{2-}$. 149

After addition of the reagents, the solution was homogenised for 2 minutes and the lamp was turned on to start the experiment. 5 mL were withdrawn before the start and at the end of each experiment to measure the transmittance of the solution by UV-visible spectrophotometry. During estrogen photolysis and AOP experiments, 1 mL of sample was withdrawn at fixed time intervals for micropollutant quantification by UHPLC. During H_2O_2 or $S_2O_8^{2-}$ photolysis experiments, the volume of samples was extended to 5 mL to determine their concentrations using a UV-visible spectrophotometer.

In any case, variations between the initial and the final volume were under 0.25% duringexperiments.

Table 3. Operating conditions in the pilot.

	Photolysis e	xperiments	UV-based AOP experiments			
	Oxidant precursors	Estrogens	Estrogens	Pharmaceuticals		
Total volume		20 :	± 0.5 L	0.5 L		
Recirculation flow rate		20 ± 0	$.5 \text{ Lmin}^{-1}$			
Solution	Drinking water	Drinking water	Drinking water or WWTP1	WWTP2		
Micropollutants	None	E1 + E2 + EE2 5 µM each	E1 + E2 + EE2 5 µM each	IBU + NAP + DCF 5 μM each		
Oxidant precursor	$H_2O_2 \text{ or } S_2O_8^{2-5}$ 5 mM	None	$H_2O_2 \text{ or } S_2O_8^{2-1}$ 1 mM	$H_2O_2 \text{ or } S_2O_8^{2-1}$ 1 mM		
Methanol	0.5% V/V	None	None	None		

161 *2.3. Sample analysis*

162 2.3.1. UV-visible spectrophotometry

163 A Shimadzu 2450 UV-visible spectrophotometer was used to:

- measure transmittances at 254 nm and 365 nm (required for UV fluence calculation),

165 - acquire the UV-visible spectra of the micropollutants and of the oxidant precursors,

166 - quantify H_2O_2 and $S_2O_8^{2-}$ during photolysis constant determination, using 167 measurements carried out at 240 nm ($\mathcal{E}_{240nm} = 38.1 \text{ L mol}^{-1} \text{ cm}^{-1}$) and 230 nm ($\mathcal{E}_{230nm} = 38.6 \text{ L}$ 168 mol⁻¹ cm⁻¹) for H_2O_2 and $S_2O_8^{2-}$ respectively.

169 *2.3.2. Micropollutant quantification*

Samples were filtered before analysis through 0.45 μ m PVDF filters (Millex HV). Analysis were performed with an UHPLC ultimate 3000+ (Thermo Fischer) system equipped with a X-Bridge BEH column (75 × 4.6 mm × 2.5 μ m) and coupled to a diode array detector. The mobile phase was a mixture of acetonitrile (ACN) and milli-Q water both acidified with 0.1% formic acid running in isocratic mode at 1.5 mL min⁻¹. One method was used to analyse the estrogens and another to analyse the mixture of pharmaceuticals. They are both described in Table 4. Limits of detection (LOD) were determined by calculation and limits of

- 177 quantification were calculated as $3.3 \times LOD$. All the samples were analysed in duplicate.
- 178 Examples of typical chromatograms are available in Figure SM2.
- 179

Table 4. UHPLC method parameters for micropollutant quantification.

UHPLC method	Estrogen method			Pharmaceutical method			
Pollutant	E1 E2 EE2			IBU	NAP	DCF	
Mobile phase ACN/H ₂ O	50/50			60/40			
Injection volume (µL)	40			20			
Column temperature (°C)		40		40			
Detection wavelength (nm)		280		226	226	281	
Retention times (min)	1.91 1.44 1.71		2.02	1.17	1.76		
Limit of detection (µM)	0.28 0.25 0.26		0.12	0.10	0.09		

180 2.4. Data processing

181 *2.4.1. UV fluence*

UV fluence $(F, mJ cm^{-2})$ corresponds to the total radiant energy incident from all directions 182 183 onto an infinitesimally small sphere of cross-sectional area dA, divided by dA according to 184 Bolton and Stefan [19]. In the studied system, the infinitesimally small sphere of cross-185 sectional area can be considered to be the targeted micropollutants or the oxidant precursors. 186 UV fluence is based on the characteristics of the lamp but also on the structure of the system 187 and on the transmittance of the effluent. Thus, it allows to compare different lamps, processes 188 or effluents. In the present study, UV fluence was used as a reference unit for degradation 189 rates.

190

2.4.2. Degradation rate constants

191 Photolysis of the estrogens and of the oxidant precursors followed first order rates that were 192 fitted by the following equation: $\ln \frac{c}{c_0} = -k'_p F$, where C_0 and C are respectively the initial 193 concentration and the concentration at UV fluence F of the compound of interest (μ M) and 194 k'_p the photolysis first order rate constant (cm² mJ⁻¹) which depends on the UV fluence 195 received by the effluent.

196 In AOPs, micropollutant degradation followed pseudo-first order rates. Targets can be 197 degraded by both photolysis and oxidation by the free radicals. In the present study, the radicals are HO' or SO_4^{-} , generated by the homolytic cleavage of H_2O_2 or $S_2O_8^{2-}$ respectively (each of them generates two identical radicals). The two modes of degradation can be distinguished in the following pseudo-first order rate equation, as proposed by Sharpless et Linden [20]:

202 $\ln \frac{c}{c_0} = -(k'_p + k'_{ox})F = -k'F$, where k'_{ox} is the pseudo-first order rate constant of 203 radical-based oxidation and k' is the overall pseudo-first order rate constant. k'_{ox} depends on 204 both the steady-state concentration of the radical and on the second order reaction rate 205 between the oxidative radical and the compound of interest [21]. In the present study, k'206 values were determined from UV-based AOP experiments and k'_{ox} values were calculated as 207 the difference between k' and k'_p .

208 The error bars associated to degradation constants equal to 3σ , derived from the scattering of 209 the experimental data around the fit curves (intra-series variability).

210 2.4.3. Electrical energy per order

The Electrical Energy per Order (E_{EO}) is the electrical energy (kWh) necessary to reduce the concentration of a contaminant by one order of magnitude in one m³ of effluent [22] (Bolton *et al.*, 2001). It is often calculated according to the following equation [23, 24]: $E_{EO} =$ $\frac{P \cdot t \cdot 1000}{V \cdot \log(\frac{C_i}{C_f})}$, where *P* is the lamp power (kW), *t* is the time of irradiation (h), V is the volume of

treated effluent (L), C_i and C_f are the initial and final concentrations of the target molecule (expressed in µmol L⁻¹ in this paper). This quantity is a useful indicator for comparing photoactivated processes. It is generally considered that a photoactivated process may be economically feasible if its E_{EO} value is less than 10 kWh m⁻³ order⁻¹ [25].

Experimental data used to calculate E_{EO} can be seen in Table SM1, only E_{EO} values are presented in the Results and discussion section.

221 **3. Results and discussion**

3.1. Estrogen and oxidant precursor photolysis

223 The molar absorption coefficient (\mathcal{E}_{λ}) and the quantum yield (Φ_{λ}) are the two parameters that account for the photolysis efficiency of a compound. The molar absorption coefficient 224 225 governs the absorption of a photon by the molecule at the wavelength of interest and the 226 photolysis quantum yield (number of photolysed molecules divided by the number of photons absorbed) depends on the photochemical change that follows photon absorption [26]. Thus, 227 228 the photolysis quantum yield influences the quantum yield for the generation of photolysis by-229 products. In the present paper, the modelling of degradation kinetics is not based on these two 230 parameters, but they are used to comment qualitatively on the degradation constants 231 calculated from experimental data.

Molar absorption coefficients of H_2O_2 and $S_2O_8^{2-}$ and of the targeted estrogens (E1, E2 and 232 233 EE2) within the UV range are depicted in Figure 2. Molar absorption coefficients at the wavelengths of interest and quantum yields for the production of HO' and SO₄. (from H_2O_2) 234 and $S_2O_8^{2-}$ photolysis, respectively) found in the literature are reported in Table 5. No 235 236 quantum yield values for the production of both radicals at 365 nm (maximum emission 237 wavelength of the UVA lamp) were found in the literature, so the values reported in Table 5 238 correspond to the wavelength found closest to 365 nm, i.e. 351 nm. As shown by Hermann 239 (2007), quantum yield decreases with increasing the wavelength of the photolysis light. This 240 decrease is barely noticeable in the case of HO' formation with quantum yield values from 1.0 241 to 0.96 when wavelength varies from 254 to 351 nm while it is much more significant in the case of SO_4 formation with quantum yield values from 1.4 to 0.5 in the same range of 242 wavelength. It can therefore be assumed that $\Phi_{365nm}(HO') \simeq \Phi_{351nm}(HO')$ while $\Phi_{365nm}(SO_4')$ 243 $<\Phi_{351nm}(SO_4^{-})$ so that the ratio $\Phi_{365nm}(HO^{-})/\Phi_{365nm}(SO_4^{-})$ can be considered greater than 1.9 244 245 for the comparison of quantum yields for the two radicals under UVA. Under UVC, the ratio 246 $\Phi_{254nm}(HO')/\Phi_{254nm}(SO_4')$ equals 0.8.



Figure 2. Molar absorption coefficients (\mathcal{E}) of E1, E2 and EE2 and of H_2O_2 and $S_2O_8^{2-}$ in the UV range at circumneutral pH.

250Table 5. Molar absorption coefficients (ε) of estrogens and oxidant precursors and quantum yields for radical251production (Φ) from the photolysis of oxidant precursors under UVC and UVA.

	$E (M^{-1} cm^{-1})$						Φ (mol e	Φ (mol ein ⁻¹)	
	H_2O_2	$S_2O_8^{2-}$	E1	E2	EE2		HO.	SO_4	
UVA	< 0.3	< 0.5	< 10	< 10	< 10	UVA	$0.96 \pm 0.04^{[27]}$	$0.5 \pm 0.1^{[27]}$	
(365 nm)						(351 nm)			
UVC	15.4	21.3	261	175	175	UVC	$1.15 \pm 0.05^{[28]}$	$1.4 \pm 0.1^{[29]}$	
(254 nm)						(254 nm)			

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249

253 *3.1.2. Photolysis rate constants of the oxidant precursors*

As seen in Figure 2, molar absorption coefficients follow the same trend in the UV range for both H_2O_2 and $S_2O_8^{2-}$: they are not significant between 400 and 350 nm and increase exponentially from 350 to 200 nm. According to Table 5, both oxidant precursors allow higher quantum yields for the production of free radicals under UVC than under UVA radiation. Therefore, although it was reported in the literature that UVA radiation is efficient for their activation [9, 30], faster photolysis is expected under UVC radiation for bothmolecules.

At 254 nm, the molar absorption coefficient of $S_2O_8^{2-}$ is 1.4 times higher than that of H_2O_2 and the quantum yield for the production of SO_4^{-} is 1.2 times higher than that of HO[•] (Table 5). Therefore, faster production of SO_4^{-} is expected. At 365 nm, a higher quantum yield for the production of HO[•] is expected compared to SO_4^{-} , as suggested by values reported in the literature at 351 nm. However, molar absorption coefficients were too low to be determined, not allowing for the assessment of photolysis outcomes.

267 Photolysis first order rate constants of H_2O_2 and $S_2O_8^{2-}$ in the experimental facility are 268 reported in Table 6. As expected, they are higher under UVC than under UVA radiation (3.5 269 and 8.8 times for H_2O_2 and $S_2O_8^{2-}$ respectively), causing faster generation of the subsequent 270 free radicals under UVC radiation. The photolysis of $S_2O_8^{2-}$ is about 1.2 and 3.4 times faster 271 than that of H_2O_2 , under UVA and UVC radiation respectively. Therefore, the generation of 272 SO_4^- is expected to be faster than that of HO⁻ regardless of the wavelength.

273

Table 6. Photolysis first order rate constants (k'_p) of H₂O₂ and S₂O₈²⁻ in the system.

	$k'_p (\mathrm{cm}^2 \mathrm{mJ}^{-1})$					
	H_2O_2	$S_2O_8^{-2-}$				
UVA	$4.36 \pm 0.30 imes 10^{-5}$	$5.25 \pm 0.51 imes 10^{-5}$				
UVC	$1.54 \pm 0.02 imes 10^{-4}$	$4.61 \pm 0.26 \times 10^{-4}$				

274

3.1.3. Photolysis of the estrogens

According to Figure 2, E1, E2 and EE2 molar absorption coefficients are very similar at all
wavelengths. They have a similar absorption band from 300 to 250 nm and molar absorption
coefficients increase exponentially in a similar way from 250 to 200 nm. However, at 254 nm,
E is 1.5 times higher for E1 than for E2 and EE2. Moreover, according to Huang et al. [31],
E1 has a 3 to 4 time higher quantum yield than E2 and EE2 at 254 nm. Therefore, faster
photolysis of E1 is expected compared to that of E2 and EE2 at this wavelength. At 365 nm,

molar absorption coefficients are not significant for the three estrogens and to the best of ourknowledge, their quantum yields at this wavelength were not reported in the literature.

283 Table 7 depicts the first order rate constants of E1, E2 and EE2 in the pilot (experimental data in the form of C/C_0 curves can be seen in Figure SM3 and Figure SM4 for UVA and UVC 284 285 respectively). First of all, the estrogens were photolysed under UVA radiation despite very 286 low molar absorption coefficients. Constants are of the same order of magnitude for the three estrogens, ranging from 8.4×10^{-6} to 1.9×10^{-5} cm² mJ⁻¹ for E1 and EE2 respectively. They 287 288 reflect very slow photolysis and less than 2% of the initial concentrations are degraded at 1000 mJ.cm², the maximum relevant UV fluence in AOPs [32], corresponding to 41 min in 289 290 the pilot. Then, higher photolysis rates of the three estrogens were observed under UVC 291 radiation. E2 and EE2 photolysis are 3 to 4 times faster and that of E1 is 113 times faster. As 292 seen previously, faster photolysis of E1 under UVC radiation was expected given its higher \mathcal{E}_{254nm} and Φ_{254nm} values. Nevertheless, the photolysis remains slow under UVC radiation with 293 only 3 to 4% degradation for E2 and EE2 at 1000 mJ cm², whereas E1 was degraded by 62%. 294 If photolysis may take part in the global degradation of estrogens during AOPs, UV 295 296 irradiation cannot be considered as an effective treatment, whether it is under UVA or UVC radiation. 297

298

Table 7. Photolysis of E1, E2 and EE2 in the system: k'_p and E_{E0} values.

		E1	E2	EE2
k'_p	UVA	$8.4\pm3.0\times10^{\text{-6}}$	$1.2\pm0.2\times10^{\text{-5}}$	$1.9 \pm 0.1 \times 10^{-5}$
$(\mathrm{cm}^2 \mathrm{mJ}^{-1})$	UVC	$9.6\pm0.5\times10^{\text{4}}$	$4.8 \pm 0.3 imes 10^{-5}$	$6.4 \pm 0.2 \times 10^{-5}$
E_{EO}	UVA	424.8	223.5	145.9
$(kWh m^{-3} order^{-1})$	UVC	2.1	47.1	31.8

299

These considerations are confirmed by the values of E_{EO} reported in Table 7: with UVA, it takes between one hundred and four hundred kWh to reduce the concentration of each estrogen in a m³ of drinking water by an order of magnitude, which far exceeds the energy 303 consumption compatible with economic feasibility. With UVC, lower E_{EO} values are 304 obtained, of the order of several tens for E2 and EE2, which remains higher than the threshold 305 value of 10 kWh m⁻³ order⁻¹, even if photolysis alone could be economically viable for E1 306 hormone degradation.

307 *3.2. Estrogen degradation in drinking water in various AOPs*

Pseudo-first order rate constants (k') of the estrogens in drinking water were calculated from experimental data (available as C/C₀ curves in Figure SM3 and Figure SM4 for UVA and UVC respectively) and are shown Table 8 as well as associated oxidation constants k'_{ox} calculated as the difference between k' and k'_p (reported in Table 7). The contribution of oxidation to the global degradation of the targets ($\%_{ox}$) was also calculated and is presented in Table 8, the complement to 100 corresponding to the contribution of photolysis.

314 Table 8. Pseudo-first order degradation constants (k') of E1, E2 and EE2 in the different processes with the 315 associated oxidation constants (k'_{ox}) and their degradation rates at 1000 mj.cm⁻².

Dediction	Owidant		Rate constants ($cm^2 mJ^{-1}$)			Degradation
Kaulation	Oxidant	Estrogen	1./	1/	% _{ox}	at 1000 mJ cm ⁻²
type	precursor		К	κ _{ox}		(%)
		E1	2.2×10^{-5}	1.4×10^{-5}	64	2.2
	H_2O_2	E2	3.3×10^{-5}	2.0×10^{-5}	61	3.2
UVA		EE2	3.5×10^{-5}	1.6×10^{-5}	46	3.4
0 VII	S ₂ O ₈ ²⁻	E1	2.1×10^{-4}	2.1×10^{-4}	100	19
		E2	2.8×10^{-4}	2.7×10^{-4}	96	24
		EE2	3.0×10^{-4}	$2.8 imes 10^{-4}$	93	26
		E1	1.7×10^{-3}	7.2×10^{-4}	42	81
	H_2O_2	E2	9.4×10^{-4}	8.9×10^{-4}	95	61
UVC		EE2	9.5×10^{-4}	8.9×10^{-4}	94	61
		E1	1.1×10^{-2}	1.0×10^{-2}	91	100
	$S_2O_8^{2-}$	E2	1.1×10^{-2}	1.1×10^{-2}	100	100
		EE2	1.1×10^{-2}	1.1×10^{-2}	100	100

Firstly, as expected, UVC radiation allows for 30 to 80% faster degradation, depending on the oxidant precursor and on the estrogen. k' ranges from 2.2 \pm 0.2 \times 10⁻⁵ to $3.0 \pm 0.2 \times 10^{-4}$ cm² mJ⁻¹ under UVA and from $9.4 \pm 0.4 \times 10^{-4}$ to $1.1 \pm 0.1 \times 10^{-3}$ cm² mJ⁻¹ under UVC radiation. Under UVA radiation, k' are ranked as follows regardless of the oxidant precursor: E1 < E2 < EE2. On the other hand, under UVC radiation, k' are similar in the presence of S₂O₈²⁻ whereas it is almost twice as high for E1 than for E2 and EE2 in the presence of H₂O₂.

When comparing the oxidant precursors, k' are 7 to 12 times higher with S₂O₈²⁻ than with H₂O₂ regardless of the UV type for E2 and EE2 and under UVA only for E1. Under UVC radiation, k'_{E1} is only about 5 times faster with S₂O₈²⁻ than with H₂O₂.

In the UVA/H₂O₂ process, k' goes from $2.2 \pm 0.2 \times 10^{-5}$ to $3.5 \pm 0.3 \times 10^{-5}$ cm² mJ⁻¹ with 46 327 to 64% of the degradation achieved by oxidation. These close results are attributed to similar 328 329 photolysis constants of the estrogens (Table 7) and similar second order rate constants (from 1.8 to 2.9×10^{10} M⁻¹ s⁻¹) between HO and the estrogens [9]. When using S₂O₈²⁻, k' values 330 increase by $89 \pm 1\%$ and are similar between the estrogens, ranging from 2.1 to 331 3.0×10^{-4} cm² mJ⁻¹, due to close second order rate constants (from 1.8 to 4.1×10^{9} M⁻¹ s⁻¹) 332 between SO₄^{\cdot} and the estrogens [9]. This increase is attributed to higher k'_{ox} thanks to faster 333 photolysis of $S_2O_8^{2-}$ compared to H_2O_2 (× 1.2) (see Table 6). As a consequence, the 334 contribution of oxidation increases, being equal to or greater than 93%. 335

Under UVC radiation, the degradation of the estrogens is accelerated. In the presence of H₂O₂, k' are from 27 to 77 times higher than those obtained under UVA. In addition to faster estrogen photolysis, H₂O₂ photolysis is 3.5 times faster under UVC than under UVA (Table 7). k'_{E2} and k'_{EE2} are similar with a contribution of oxidation reaching 95 and 94% respectively. However, k'_{E1} is almost twice as high as k'_{E2} and k'_{EE2} . It is observed that k'_{ox} are

of the same order of magnitude for the three estrogens, from 7.2 to $8.9 \times 10^{-4} \text{ cm}^2 \text{ mJ}^{-1}$. 341 342 Therefore, faster degradation of E1 is attributed to its high photosensitivity under UVC radiation. Similar trends are observed with the use of $S_2O_8^{2-}$: k' are from 39 to 52 times higher 343 under UVC radiation due to faster oxidation. For E2 and EE2, the increase in k'_{ox} is so high 344 that k'_p becomes negligible. Regarding E1, k'_p remains noticeable (about 10% of total 345 degradation). However, a lower k'_{ox} leads to similar k' than that of E2 and EE2. Finally, 346 347 oxidation plays a major role in E2 and EE2 degradation under UVC regardless of the oxidant 348 precursor whereas the predominant phenomenon in the degradation of E1 varies depending on 349 the oxidant precursor.

Estrogen degradation rates at 1000 mJ cm⁻² are reported in Table 8. With UVC/S₂O₈²⁻, the 350 three estrogens are fully degraded. On the other hand, the UVA/H2O2 process provides less 351 than 4% degradation at 1000 mJ cm⁻² and does not seem viable. As a consequence, it was not 352 studied in the following parts of the work. Contrasted results are observed with $UVA/S_2O_8^{2-1}$ 353 354 (19 to 26% degradation) and UVC/H₂O₂ (61 to 81% degradation). With the aim of promoting 355 the use of UVA rather than UVC radiation in photoactivated AOPs, coupling UVA radiation to $S_2O_8^{2-}$ could be relevant since it induces encouraging results compared to the UVC/H₂O₂ 356 357 process.

The values of E_{EO} calculated for estrogens degradation in drinking water shown in Table 9 lead to the same conclusions. Using UVC whatever the free radical precursor seems to be economically feasible with E_{EO} values between 0 and 2 kWh m⁻³ order⁻¹. So it seems worthwhile to study the UVC-based AOPs with a complex matrix such as WWTP effluent, even if these conditions may be less favorable. With the UVA/S₂O₈²⁻ process, E_{EO} values are a little bit higher, in the upper range of acceptable values. It is therefore important to determine whether the switch to real matrix leads to a significant increase in E_{EO} values or not. Finally,

- 365 E_{EO} values obtained with the UVA/H₂O₂ process are around hundred for the three estrogens in
- 366 drinking water, so there is no point in going any further with this process.
- 367

Table 9. Values of E_{EO} for estrogens degradation by photooxidation in different matrices.

Radiation Oxidant type precursor		Estrogen	E (kWh m Drinking water	eo 1 ⁻³ order ⁻¹) WWTP effluent	Ratio $E_{EO}(DW)$ $\overline{E_{EO}(WWTP)}$	
		E1	126.6	-	-	
	H_2O_2	E2	81.3	-	-	
T 137 A		EE2	84.4	-	-	
UVA	$S_2O_8^{2-}$	E1	10.3	59.8	5.8	
		E2	7.6	55.1	7.2	
		EE2	7.3	49.4	6.7	
		E1	1.3	2.1	1.6	
	H_2O_2	E2	2.2	3.5	1.6	
UVC		EE2	2.1	3.2	1.5	
	$S_2O_8^{2-}$	E1	0.2	0.9	5.0	
		E2	0.1	0.9	7.7	
		EE2	0.1	0.9	7.1	

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3.3. Process comparison in a WWTP effluent

After the study of UV-based AOPs in a simple matrix, it is necessary to implement them in a real matrix. Real effluents may indeed contain species that absorb UV radiations, react with radical precursors and/or with free radicals, leading to poorer performance of the process. Furthermore, it has been shown that photolysis and oxidation are compound dependent. Thus, it seems interesting to assess the degradation of another kind of micropollutants. This part, dedicated to the degradation of micropollutants in spiked WWTP effluents, firstly focuses on the estrogens and then on a mixture of three pharmaceuticals.

378 3.3.1

3.3.1. Estrogen degradation

WWTP effluent 1 collected at the outlet of a conventional treatment plant (see Table 2 for more details) and spiked with the three estrogens was used to assess the performance of the $UVA/S_2O_8^{2-}$, UVC/H_2O_2 and $UVC/S_2O_8^{2-}$ processes (see Table 3 for operating conditions). Pseudo-first order degradation rate constants of the estrogens are presented and compared to those measured in drinking water in Figure 3 (data is available in Table SM2, experimental data is available as C/C_0 curves in Figure SM5).

385 First of all, estrogen degradation rates in WWTP effluent follow the same behaviours as described previously in drinking water: $S_2O_8^{2-}$ induces faster degradation than H_2O_2 and UVC 386 is more efficient than UVA radiation (with $S_2O_8^{2-}$ only since UVA/H₂O₂ was not 387 implemented). However, k' are lower in the WWTP effluent than in drinking water. Inhibition 388 389 percentages are presented in Figure 3. They were calculated by comparing the degradation 390 rate constants obtained in the WWTP effluent to those obtained in drinking water. In the presence of $S_2O_8^{2-}$ and regardless of the type of radiation, k' are reduced by 76 to 80%. 391 392 However, in the UVC/H₂O₂ process, degradation rates are only inhibited by 27, 30 and 12% 393 for E1, E2 and EE2 respectively. Based on these results, process performances seem to be much more affected in a real matrix when $S_2O_8^{2-}$ is used compared to H_2O_2 . 394

In the literature, the reactivity of H_2O_2 and $S_2O_8^{2-}$ with the WWTP effluent components 395 396 (mainly organic matter and inorganic anions) was not reported to be significant. The 397 inhibition in a WWTP effluent is rather probably due to the scavenging of the oxidative 398 radicals by the organic matter and inorganic anions such as Cl^{-} , NO_{3}^{-} and HCO_{3}^{-} [9, 33, 34]. 399 Results obtained in the present study suggest that the scavenging of the radicals by the matrix components is stronger for SO_4 . than for HO. In both matrices under study, carbonate 400 concentrations are similar. However, the total organic carbon of the effluent is 7.5 $mg_C L^{-1}$ 401 402 whereas that of drinking water is not significant ($< 0.5 \text{ mg}_{\text{C}} \text{ L}^{-1}$). In addition, conductivity, 403 chloride and nitrate concentrations are 2.3, 10 and 4.2 times higher in the WWTP effluent respectively. These differences in matrix composition could indeed induce HO and SO4. 404 405 scavenging. Wang and Wang [35] reported in a literature review that both radicals have similar second order reaction rate constants with HCO_3^- (9 × 10⁶ M⁻¹ s⁻¹), that Cl⁻ have 406

407 negligible effect and that NO_3^- could have a scavenging impact, although its second order 408 reaction rate with HO is not reported and that with SO_4 . is negligible $(k_{SO_4^{-},NO_3^{-}}^{\prime\prime} = 2.1 \text{ M}^{-1} \text{ s}^{-1})$. Therefore, the significant decrease in efficiency of S₂O₈²⁻ observed 409 in the present study under both types of radiation could rather be attributed to radical 410 scavenging by organic matter, which would be stronger for SO_4 . This 411 412 inhibition is governed by the competition between the micropollutants of interest and organic 413 matter to react with the radicals. Second order rate constants between the radicals and the 414 organic matter were not determined in the present study. However, Lutze et al. [36] reported 415 higher reaction rates of natural organic matter with HO \cdot than with SO₄ \cdot but they only considered humic acids whereas it was previously reported in the literature that the 416 417 composition of organic matter in WWTP effluents has a large variation range which also 418 includes fulvic acids, hydrophilic acids, bases and neutral or hydrophobic neutrals for 419 example [37, 38, 39]. Regarding the reactivity between the estrogens and the radicals, Gabet 420 et al. [9] previously reported that second order rate constants are lower with SO₄. (from $1.8 \times$ 10^9 to 4.1×10^9 M⁻¹ s⁻¹) than with HO• (from 1.8×10^{10} to 2.9×10^{10} M⁻¹ s⁻¹). As a 421 consequence, SO_4 . is more likely to be scavenged by organic matter than HO, depending on 422 423 their second order reaction rates with the organic matter involved.



Figure 3. Pseudo-first order degradation rate constants of E1, E2 and EE2 (5 μ M) in a WWTP effluent compared to those in drinking water, H₂O₂ or S₂O₈²⁻ = 1 mM.

427 In drinking water, $UVA/S_2O_8^{2-}$ seemed to have potential in degrading estrogens: it induced 428 degradation rates only 3 to 8 times slower than UVC/H_2O_2 . In the WWTP effluent, this is no 429 longer the case because $UVA/S_2O_8^{2-}$ provides 12 to 24 times lower k' values than UVC/H_2O_2 .

430 Regarding UVC-based processes, $UVC/S_2O_8^{2^2}$ was by far the most competitive process in 431 drinking water with 7 to 12 times faster degradations than with H_2O_2 . In a WWTP effluent, 432 they are only 2 to 3.4 times faster than with H_2O_2 . Therefore, even if $UVC/S_2O_8^{2^2}$ still gives 433 the best results, performance indicators become of the same order of magnitude as those 434 obtained with UVC/H_2O_2 .

Unsurprisingly, the E_{E0} values reported in Table 9 show that the electrical energy required to reduce estrogens concentrations by one order of magnitude increases when aqueous matrix becomes more complex (from drinking water to WWTP effluent). However, UVC-based processes still exhibit E_{E0} values lower than 10 kWh m⁻³ order⁻¹ and even lower than 4, attesting to their economic feasibility. Based on E_{E0} , UVC/S₂O₈²⁻ is more attractive than 440 UVC/H₂O₂ with E_{E0} values two to four times lower. Regarding UVA/S₂O₈²⁻ process, 441 switching to a real matrix raises E_{E0} values (up to between 50 and 60 kWh m⁻³ order⁻¹) above 442 the economic feasibility threshold. While this excess is not strictly prohibitive for UVA 443 technologies, it does indicate that UVC-based AOPs are comparatively more economically 444 attractive.

For the two processes that use persulfate ions as radical precursors, E_{EO} values increase by a factor of between 5 and 8 as a result of the matrix change, whether with UVA or UVC, whereas this factor is around 1.5 for UVC/H₂O₂. As seen above based on kinetics considerations, the switch to a real matrix also reduces the performance of persulfate based AOPs more than that of H₂O₂ based ones.

450 *3.3.2. Pha*

3.3.2. Pharmaceutical degradation

WWTP effluent 2 collected at the outlet of the same conventional treatment plant (see Table 2 for more details) was spiked with a mixture of three pharmaceuticals, namely ibuprofen (IBU), naproxen (NAP) and diclofenac (DCF). The UVA/S₂O₈²⁻, UVC/H₂O₂ and UVC/S₂O₈²⁻ processes were carried out in the same conditions as previously. Pseudo-first order degradation rates of the mixture of pharmaceuticals are depicted in Figure 4 (data is available in Table SM3 and experimental data is available as C/C₀ curves in Figure SM6).

In all the processes, k' are significantly different between the three compounds and their ranking is similar in the three processes: $k'_{IBU} < k'_{NAP} < k'_{DCF}$. k'_{DCF} is 7 and 11 times higher than k'_{IBU} with H₂O₂ and S₂O₈²⁻ respectively and it is 5.5 times greater than k'_{NAP} with H₂O₂. However, it is less than twice k'_{NAP} with S₂O₈²⁻. As observed for the estrogens, both UVC processes provide faster degradation rates than UVA/S₂O₈²⁻ (from 10 to 63 times with H₂O₂ and from 38 to 56 times with S₂O₈²⁻). However, degradation rates are of the same order of magnitude under UVC radiation with the two oxidant precursors. They are only 1.3 and 3.7 464 times faster with $S_2O_8^{2-}$ for DCF and NAP respectively and the degradation of IBU is on the 465 contrary 1.2 times slower with $S_2O_8^{2-}$ than with H_2O_2 .

Firstly, the difference in degradation rates between the three pharmaceuticals is going to be 466 discussed. Under UVC radiation, DFC is highly photolysable: Fu et al. [40] reported a high 467 468 photolysis rate of DCF with 92% degradation after 600 s of exposure in their system whereas 469 NAP and IBU were degraded by 52 and 28% respectively. Under UVA radiation, low 470 photolysis is expected in view of the global degradation results reported in Figure 4. 471 However, it has not been studied, to the best of our knowledge. Regarding oxidation, second order rate constants (k'') all are of the same order of magnitude (Table 10). However, they 472 473 follow the same trend as k': those of DCF are equal to or higher than those of NAP which are 474 higher than those of IBU. Therefore, the differences in pseudo-first order degradation rates 475 between the pharmaceuticals are attributed to both their different photo-sensitivities and their 476 second order rate constants with HO• and SO4•.



Table 10. Second order reaction constants between the radicals and IBU, NAP and DCF.

	IBU	NAP	DCF
k''_{HO} (M ⁻¹ s ⁻¹)	$5.57 imes 10^{9}$ ^[41]	9.05×10^{9} ^[42]	9.29×10^{9} ^[43]
$k_{SO_4}^{\prime\prime}$ (M ⁻¹ s ⁻¹)	$1.32 \times 10^{9} ^{[41]}$	$5.64 imes 10^{9}$ ^[42]	$9.2 \times 10^{9} ^{[44]}$

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Regarding process efficiency, faster degradation under UVC radiation is attributed to both faster pharmaceutical photolysis and radical generation. Moreover, as seen previously, better degradation in the presence of $S_2O_8^{2-}$ is attributed to the faster generation of SO_4 .⁻ compared to HO.⁻. Under UVC radiation, only the degradation of IBU is faster in the presence of H_2O_2 than with $S_2O_8^{2-}$. This is due to $k''_{HO,,IBU}$ which is more than 4 times higher than $k''_{SO_4^{-},IBU}$. The same trend is observed with NAP whose second order rate constant is 1.6 times higher with HO.⁻ compared to SO_4 .⁻. However, the competition between the different species or the 486 faster generation of SO_4 . allows NAP to be degraded faster in the UVC/S₂O₈²⁻ process 487 compared to UVC/H₂O₂.



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 $\begin{array}{l} 489\\ 490 \end{array} \mbox{ Figure 4. Pseudo-first order degradation rate constants of IBU, NAP and DCF (5 \mbox{μM$}) in a WWTP effluent, H_2O_2 or $S_2O_8^{2-} = 1$ mM. \end{array}$

491 E_{EO} calculated for the degradation of pharmaceuticals are shown in Table 11. As already seen 492 with estrogens, UVC-based AOPs exhibit more favorable values of E_{EO} (lower than 10 kWh m⁻³ order⁻) than UVA-based one. With persulphate ions as radical precursor and irrespective 493 494 of UV radiation energy, the E_{E0} of IBU is significantly higher than that of NAP and DCF, 495 which are of the same order of magnitude. E_{EO} obtained from UVC/H₂O₂ experiments are less contrasted. It is worth noticing that when comparing the highest and the lowest E_{EO} values for 496 497 a given AOP, the ratios vary from 7 to 20 in the case of pharmaceuticals attesting a high 498 degree of variability depending on the molecules, whereas they were much less dispersed, 499 from 1.4 to 2.0, in the case of hormones which have fairly similar molecular structures.

500 Table 11. Values of E_{E0} for pharmaceuticals degradation by photooxidation in WWTP effluent 2.

Radiation type	Oxidant precursor	Pharmaceutical	E_{EO} (kWh m ⁻³ order ⁻¹)	
		IBU	203.1	
UVA	$S_2O_8^{2-}$	NAP	23.3	
		DCF	15.5	
	H_2O_2	IBU	2.1	
		NAP	1.7	
		DCF	0.3	
UVC		IBU	4.0	
	$S_2O_8^{2-}$	NAP	0.5	
		DCF	0.2	

502 3.3.3. Removal efficiencies at 1000 mJ cm⁻²

Removal efficiencies at 1000 mJ cm⁻² in the three processes are depicted in Table SM2 for estrogens and in Table SM3 for the pharmaceuticals.

The UVA/ $S_2O_8^{2-}$ process only allowed weak degradation of the model micropollutants. The 505 506 estrogens were not degraded by more than 6% and the pharmaceuticals by 17%. On the other 507 hand, UVC radiation allowed satisfactory or good removal efficiencies at 1000 mJ cm⁻², depending on the model micropollutant and the oxidant precursor. In the presence of H_2O_2 , 508 509 the estrogens were degraded from 43 to 71% and IBU, NAP and DCF were degraded by 66, 75 and 100% respectively. In the presence of $S_2 O_8^{2-}$, the three estrogens underwent better 510 511 degradation with removal efficiencies reaching 90 \pm 1%. NAP also underwent better 512 degradation and was almost completely degraded (99%) and DCF was still completely 513 removed, whereas IBU was only degraded by 58%, which is slightly poorer than the 514 degradation performances allowed by the UVC/H₂O₂ process, due to a lower k', as discussed in section 3.3.2. As a consequence, the better performances of the UVC/S₂O₈²⁻ are clear for 515 516 the estrogens and NAP. However, both UVC processes are comparable for the degradation of 517 DCF which is mainly photodegraded and IBU reaches slightly higher degradation in the 518 presence of H₂O₂, depicting the importance of the nature of the target in the process efficiency 519 assessment.

520 In Switzerland, where a regulation regarding the removal of micropollutants in WWTPs is 521 applicable, it imposes 80% removal on a selection of micropollutants over the complete treatment process. In the present study, the $UVC/S_2O_8^{2-}$ process provides alone such 522 523 degradation for 5 of the 6 studied compounds and although the UVC/H₂O₂ process does not 524 allow such performances, it could significantly increase the overall micropollutant removal in a WWTP when used as a tertiary treatment. 525

526

4. Conclusion

The following main conclusions can be drawn from this study about the feasibility of 527 replacing UVC by UVA in AOPs to degrade micropollutant. Firstly, experiments carried out 528 529 in drinking water as a simplified matrix with a mixture of estrogens showed that UVA is less efficient than UVC in photolyzing both the radical precursors (H_2O_2 or $S_2O_8^{2-}$) and targeted 530 531 compounds, which results in lower degradation rates as well as poorer performance at a given UV fluence. Based on E_{EO} calculations, UVA/H₂O₂ seems not economically feasible unlike 532 533 other AOPs.

Experiments carried out with estrogens- or pharmaceuticals-spiked WWTP effluents showed 534 that in the presence of a complex matrix, the UVA/S₂ O_8^{2-} process is no longer feasible with 535 values of E_{EO} higher than threshold value. For all AOPs, performance decreases drastically in 536 WWTP matrix, but the UVC-based processes remain economically feasible with satisfactory 537 538 micropollutant degradation. Persulphate ions still provide better degradation performances than H₂O₂, even though inhibition due to matrix change, expressed as a % relative to drinking 539 540 water, is stronger, showing a higher scavenging effect of SO_4 . than of HO· by organic matter.

541 Since the efficiency of a radical precursor is both compound- and matrix-dependent, further 542 experiments on a larger panel of micropollutants would be required in order to confirm $S_2O_8^{2-}$ 543 better efficiency.

The E_{EO} is a useful tool to compare AOPs, and especially to compare UVA- and UVCprocesses. Nevertheless, it should be completed by another parameter that would enable a fair comparison of radical precursors to be integrated in a technico-economical indicator. For example, the price of a reagent is not the only parameter that induces cost, its implementation has also to be taken into account. However, in view of the experiences carried out in the present study, a more detailed technical and economic approach seems premature.

Finally, if the use of mercury-based UVA lamps is ruled out by the results of the present 550 551 study, there are other UVA radiation sources that could allow for the implementation of less 552 energy consuming processes and for the consideration of UV fluences greater than 1000 mJ cm⁻² (defined for UVC mercury-based lamps). UVA-light emitting diodes (LEDs) 553 554 are one of them. LEDs have been an emerging light source over the past years and they are 555 known for their high energy efficiency, robustness, clean composition and potential for long 556 lifetimes [45]. UVA-LEDs are particularly interesting because they can be up to 15 times 557 more energy efficient than UVA mercury lamps [46], on the contrary to UVC-LEDs which 558 have low energy efficiency [47]. Another solution for UVA-based processes are solar-driven 559 systems that would allow considering greater energy requirements to reach complete 560 degradation of the targets because solar light is a free and clean energy. However, their major 561 drawback remains process implementation: despite the availability of solar light concentrator, 562 designing a system able to provide appropriate UV fluence for the degradation of 563 micropollutants with solar radiation remains nowadays challenging.

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5. Declaration of Competing Interest

566 All authors declare no conflict of interest.

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Supplementary Materials Pilot-scale assessment of the viability of UVA radiation for H₂O₂ or S₂O₈²⁻ activation in advanced oxidation processes Anaëlle Gabet^{1,2}, Christine de Brauer¹, Gilles Mailhot², Marcello Brigante², Hélène Métivier¹ ¹ Univ Lyon, INSA Lyon, DEEP, EA7429, 69621 Villeurbanne, France ² Université Clermont Auvergne, CNRS, Clermont Auvergne INP, Institut de Chimie de Clermont-Ferrand, F-63000 Clermont-Ferrand, France *corresponding author: helene.metivier@insa-lyon.fr

Figure SM1. UVA lamp emission spectrum (Philips).







Initial concentration of estrogens: 5 μM each; initial concentration of radical precursor (hydrogen peroxide (H2O2) or persulphate ions (PS)): 1 mM; aqueous matrix is drinking water (Table 2).





Initial concentration of estrogens: 5 μM each; initial concentration of radical precursor (hydrogen peroxide (H2O2) or persulphate ions (PS)): 1 mM; aqueous matrix is drinking water (Table 2).



788

789 Initial concentration of estrogens: 5 μM each; initial concentration of radical precursor (hydrogen peroxide (H2O2) or persulphate ions (PS)): 1 mM; aqueous matrix is WWTP effluent 1 (Table 2).



Initial concentration of pharmaceuticals: 5 μM each; initial concentration of radical precursor (hydrogen peroxide (H2O2) or
 persulphate ions (PS)): 1 mM; aqueous matrix is WWTP effluent 2 (Table 2)

Matrix	Radiation	Oxidant	Time	Target	C _i	C_f	E _{EO}		
WIGUIX	type	precursor	(min)	molecule	(µM)	(µM)	$(kWh m^{-3} order^{-1})$		
	Estrogens								
				E1	4.09	3.82	424.8		
	UVA	None	420	E2	4.60	4.04	223.5		
				EE2	4.38	3.59	145.9		
				E1	4.21	0.05	2.1		
	UVC	None	90	E2	4.29	3.52	47.1		
				EE2	4.49	3.35	31.8		
5				E1	4.20	3.34	126.6		
'ate		H_2O_2	420	E2	4.50	3.15	81.3		
50 A	ΙWA			EE2	4.57	3.24	84.4		
lkin	UVA			E1	4.32	0.87	10.3		
Drin		$S_2O_8^{2-}$	240	E2	4.51	0.51	7.6		
				EE2	4.61	0.48	7.3		
				E1	4.72	0.44	1.3		
	UVC	H_2O_2	30	E2	4.86	1.17	2.2		
				EE2	4.75	1.09	2.1		
		$S_2O_8^{2-}$	5	E1	3.99	0.25	0.2		
				E2	4.26	0.06	0.1		
				EE2	5.35	0.09	0.1		
		$S_2O_8^{-2}$	360	E1	4.38	2.89	59.8		
	UVA			E2	4.38	2.79	55.1		
nt 1				EE2	4.78	2.89	49.4		
lue				E1	4.75	0.23	2.1		
eff		H_2O_2	60	E2	4.85	0.81	3.5		
dT'				EE2	5.07	0.71	3.2		
M A	UVC			E1	4.1	1.89	0.9		
-		$S_2O_8^{2-}$	7	E2	4.34	1.99	0.9		
				EE2	4.78	2.14	0.9		
		•	Pl	narmaceutica	als				
				IBU	5.42	4.79	203.1		
	UVA	$S_2O_8^{2-}$	360	NAP	4.71	1.62	23.3		
nt 2				DCF	4.34	0.87	15.5		
luei				IBU	5.70	2.67	2.1		
eff		H_2O_2	15	NAP	5.38	2.18	1.7		
dT'	IWC			DCF	4.70	0.03	0.3		
M A				IBU	5.15	4.53	4.0		
-		$S_2O_8^{2-}$	5	NAP	4.03	1.38	0.5		
				DCF	4.03	0.46	0.2		

802 *Table SM2. Pseudo-first order degradation constants of E1, E2 and EE2 in the different processes with two different matrices and the degradation rates at 1000 mJ cm⁻² in WWTP effluent 1.*

			Drinking	WWTP effluent 1	
			water		
Radiation	Oxidant	Estragon	Rate constants k'		Degradation at 1000 mJ cm ⁻²
type	precursor	Estrogen	$(\mathrm{cm}^2 \mathrm{mJ}^{-1})$		(%)
UVA	$S_2O_8^{2-}$	E1	2.1×10^{-4}	5.2×10^{-5}	5
		E2	2.8×10^{-4}	5.5×10^{-5}	5
		EE2	3.0×10^{-4}	6.3×10^{-5}	6
UVC	H ₂ O ₂	E1	1.7×10^{-3}	1.2×10^{-3}	71
		E2	9.4×10^{-4}	6.6×10^{-4}	48
		EE2	9.5×10^{-4}	$8.4 imes 10^{-4}$	43
	S ₂ O ₈ ²⁻	E1	1.1×10^{-2}	2.3×10^{-3}	90
		E2	1.1×10^{-2}	2.3×10^{-3}	90
		EE2	1.1×10^{-2}	2.4×10^{-3}	91

807 Table SM3. Pseudo-first order degradation constants of IBU, NAP and DCF in the different processes with WWTP effluent 2 as a matrix and the degradation rates at 1000 mJ cm^{-2} .

Radiation	Oxidant		Rate constants k'	Degradation at 1000 mJ cm ⁻²
type	precursor	Pharmaceuticais	$(\mathrm{cm}^2 \mathrm{mJ}^{-1})$	(%)
UVA		IBU	$1.7 imes 10^{-5}$	2
	S ₂ O ₈ ²⁻	NAP	$1.3 imes 10^{-4}$	13
		DCF	$1.8 imes 10^{-4}$	17
UVC	H ₂ O ₂	IBU	1.1×10^{-3}	66
		NAP	1.4×10^{-3}	75
		DCF	$7.7 imes 10^{-3}$	100
	S ₂ O ₈ ²⁻	IBU	$8.7 imes 10^{-4}$	58
		NAP	$5.1 imes 10^{-3}$	99
		DCF	$1.0 imes 10^{-2}$	100