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A biomechanical confirmation of the relationship between critical shoulder angle (CSA) and articular joint loading.

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and articular joint loading

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4 Abstract

5 **Background**: The Critical Shoulder Angle (CSA) has been shown to be correlated with

shoulder disease states. The biomechanical hypothesis to explain this correlation is that the

CSA changes the shear and compressive forces on the shoulder. The objective of this study is

to test this hypothesis by use of a validated computational shoulder model. Specifically, this

9 study assesses the impact on glenohumeral biomechanics of modifying the CSA.

10 **Methods:** An inverse dynamics three-dimensional musculoskeletal model of the shoulder was

used to quantify muscle forces and glenohumeral joint forces. The CSA was changed by

altering the attachment point of the middle deltoid into a normal CSA (33°), a reduced CSA

of 28°, and an increased CSA of 38°. Subject-specific kinematics of slow and fast speed

abduction in the scapular plane, and slow and fast forward flexion measured by a 3D motion

capture system were used to quantify joint reaction shear and compressive forces.

16 **Results**: Increasing the CSA results in increased superior-inferior forces (shearing forces;

integrated over the range of motion; p<0.05). Reducing CSA results in increased latero-

medial (compressive) forces for both the maximum and integrated sum of the forces over the

whole motion; p<0.01).

20 **Discussion/Conclusion**: Changes in the CSA modify glenohumeral joint biomechanics with

increasing CSA producing higher shear forces that would contribute to rotator cuff overuse,

whereas reducing the CSA results in higher compressive forces which contribute to joint

23 wear.

24 Level of evidence: Basic Science Study; Computer Modeling

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Keywords: Critical shoulder angle (CSA), glenohumeral joint, joint wear, rotator cuff,
 computational shoulder model.

The shape of the scapula and especially of the acromion has historically been considered as a potential etiology for shoulder pathologies including those of the gleno-humeral joint (GHJ). Codman ¹⁰, Armstrong ³ and Neer ²⁶ described the association of specific acromion shapes with degenerative rotator cuff tear (RCT), leading to the well-known impingement syndrome and the extrinsic mechanical conflict theory. Since then, a broader understanding of degenerative RCT physiopathology ³⁵ (ageing of the tendon, modification of local vascularization, genetic disposition) has challenged this theory, thus questioning the absolute role of the acromion shape in this process. Research over the past 15 years has continued to focus on the shape of the acromion in the coronal plane, including proposed radiological parameters to describe the lateral extension of the acromion ^{5,28}. A recent and widely cited study from Moor et al proposed the concept of the Critical Shoulder Angle (CSA) ²⁴, a measure which takes into account the tilt of the glenoid (inclination) and the lateral extension of the acromion. In a population of 279 patients, they found that the mean CSA was significantly different between a disease-free shoulder group (33.1°), an RCT group (38.0°), and a primary osteoarthritis group (OA, 28.1°). Numerous clinical observational studies have confirmed these findings ^{4,5,8,11–13,15,16,23,25,38,43}.

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The link between the clinical observations and the CSA are hypothesized to be biomechanical in nature ^{2,27,22,14,40,42}, by changing the magnitude and direction of the deltoid force. The hypothesis of this study is that an increased CSA would result in higher shearing forces that would be associated with RCT and a decreased CSA would result in higher compressive forces, associated with primary osteoarthritis.

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The objective of this study is to test the hypothesis by assessing the impact on GHJ biomechanics of modifying the CSA by use of a validated computational shoulder model.

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Material and Methods

The United Kingdom National Shoulder Model (UKNSM)

An inverse dynamics three-dimensional musculoskeletal model of the upper limb ⁹ was used to quantify muscle and glenohumeral joint forces. This model quantifies forces in 87 muscle elements, three ligaments and joint reaction forces of the sternoclavicular, acromioclavicular, scapulothoracic, glenohumeral and elbow joint (Figure 1). The analysis begins by solving the determinate inverse dynamics intersegmental moments based on measured kinematics. Then an optimization algorithm is used to minimize the sum of muscle stresses squared to solve the muscle load-sharing redundancy. The model has been validated for glenohumeral joint force measures through comparison to instrumented anatomical shoulder replacement measurements ^{7,44} for a driving task ²⁹ and other tasks of daily living ¹⁹ and for muscle forces through comparison with electromyography ¹⁸. The model is customized to each subject by scaling segment lengths and body segment parameters. ¹⁷ In brief, clavicle and scapula segments were homogeneously scaled based on relative segment lengths between model and subject. An ellipsoid represented the scapulo thoracic gliding-plane; this was nonhomogeneously scaled using an optimization procedure to minimize the difference between digitized anatomical landmarks and the final ellipsoid. A partially closed chain method is used to optimize scapula and clavicle kinematics, in which the least squares difference to the measured scapular and clavicle kinematics is minimized and the scapula medial border is constrained to not penetrate the thorax wall (represented by an elipsoid). ³²

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Tests conditions

The scapula within the UKNSM was imported into computer aided engineering software to allow the effect of medializing and lateralizing the acromion to be modelled, thus changing the CSA and therefore the three-dimensional position of the attachment point of the middle deltoid. This was implemented in the software by sketching new points and lines parallel to the plane of measurement of the CSA and coincident with the original middle deltoid attachment point. The changes were made to create 3 different CSAs: a normal CSA (33°), a reduced CSA of 28°, and an increased CSA of 38° that reflect the changes previously reported as clinically significant ²⁴.

To test the effect of different subject-specific kinematics, a previously obtained dataset of kinematics was used 20 . These kinematics were measured using a nine camera optical motion tracking system with a set of twenty-one retro-reflective markers used to track the thorax, clavicle, humerus, and forearm segments 36,37,45 . The kinematics of six healthy male subjects were used (age 25 years \pm 2 years) who each performed four motions with a 2 kg hand load to provide a resistance to motion without fatiguing the subjects. These motions were: slow and fast speed abduction (in the scapular plane), and slow and fast forward flexion 34 . Each subject performed three trials per motion. These datasets were passed through the UKNSM after appropriate subject scaling 32 .

Outcomes measures

All output measures were normalized to humero-thoracic elevation and all forces were normalized to the subject's body weight and integrated over the range of motion from 30° to 120° of humero-thoracic elevation. The following parameters were analyzed to test the effects of CSA changes on GHJ biomechanics:

- the magnitude (maximum and integrated over the whole motion) of the GHJ shearing forces
 (SF), representing the superior-inferior (SI) forces and the antero-posterior (AP) forces acting
 in the sagittal plane that are exerted on the joint during motion.
 - the magnitude (maximum and integrated over the whole motion) of the GHJ compressive

forces (CF), representing the forces acting in the frontal plane (latero-medial) that are exerted

on the joint during motion.

Statistical Analysis

Repeated measures two-way ANOVA (RM 2-Way ANOVA), with Bonferroni post-hoc correction was conducted on the results using SPSS software (2014; IBM Corp., Armonk, NY, USA). The assumptions of the RM 2-Way ANOVA method were tested for all measures. The independent variables are CSA (normal, increased, reduced) and Motion (fast and slow, forward flexion and scapular plane abduction); the dependent variables are the joint forces (integrated AP shear, max AP shear, integrated SI shear, max SI shear, integrated CF, max CF). Mauchly's test indicated that the assumption of sphericity had been violated for the main effects of CSA and Motion for several measures, therefore degrees of freedom were corrected using Greenhouse-Geisser estimates of sphericity (ε).

Results

Statistically significant differences were found for the integrated SI shear force, the integrated CF and the maximum CF (Table 1). These statistical results are presented in Figure 2. In summary, an increased CSA angle resulted in 111% higher integrated SI shear forces (p<0.05) when compared to normal. For the compressive forces, a reduced CSA angle resulted in a significant increase of the CF (integrated: 2.8% increase, p<0.01; maximum: 2.8% increase, p<0.05) compared to normal CSA and also when compared to increased CSA

(integrated: 5.5% increase, p<0.01; maximum 5.3% increase, p<0.05). There were no main 125 effects found for Motion, nor an interaction effect of Motion and CSA. 126 The mean maximum SI forces were 13% BW, 12% BW and 21% BW for reduced, normal 127 and increased CSA, respectively. The maximum CF were 132% BW, 136% BW and 129% 128 BW for reduced, normal and increased CSA, respectively. 129 130 **Discussion** 131 This is the first study to assess the effects of changes in CSA on GHJ biomechanics through a 132 computational shoulder model in order to test the mechanically-based hypothesis. The results 133 confirm the initial hypothesis based on literature 41, that is to say increasing the CSA results in 134 increased superior-inferior forces (shearing forces), whereas decreasing the CSA results in 135 increased latero-medial (compressive force) forces (Figure 3). 136 137 Our results are also consistent with those of two cadaver studies previously published about 138 139 the subject. Even if the model and analysis method are different, Vielhofer and Gerber found 140 that with an increased CSA, the ratio of glenohumeral joint shear to joint compression forces is increased (peak difference of 23% at 50° of thoraco-humeral abduction compared to a 141 normal CSA) ⁴⁰, requiring substantially increased compensatory supraspinatus loads 142 (increased by 13-33% between 33° and 37° of elevation compared to a normal CSA)¹⁴. 143 144 These cadaver studies combined with the study presented here provide simple mechanical 145 explanations for the results: 146 an increased CSA would result in a lateralized proximal deltoid insertion. 147 Consequently, the vector force of the deltoid during abduction would be more vertical, 148 requiring a greater horizontal force from the cuff to stabilize the joint (by 149

counterbalancing the shearing forces). Ultimately, this increase in muscle use could potentially, in combination with other factors, lead to a degenerative RCT in the long-term; and

• a reduced CSA would result in a medialized proximal deltoid insertion. Consequently, the vector force of the deltoid during abduction would be more oblique (resultant internal translation), which in addition to the vector force of the cuff (mostly horizontal), could increase the load (compressive forces) on the GHJ. Finally, this could lead to OA in the long-term.

It is known that small elevated mechanical loading is associated with the instigation and progression of osteoarthritis^{1,30}, suggesting that, although small in percentage terms, the statistical differences in key mechanical variables found here may also be clinical significant.

Computational simulation models are frequently used to analyze human joint biomechanics and have been validated in studies that quantified articular loading in activities of daily living, and the biomechanical consequences of a pathology, surgery, and arthroplasty ^{9,20,31,39}.

Concerning shoulder modelling, the UKNSM (formerly Newcastle Shoulder Model) ⁹ is one the oldest validated inverse dynamics-based models ³³. Body segment parameters are based on a large group of young living patients ²¹. There are limitations with such models and so, although, the model has been validated by comparison to instrumented joint replacements and electromyography, such computer simulations remain "models" and are, therefore, a surrogate of direct in-vivo biomechanical measurements.

Apart from technical considerations of the computational model, this study has some other limitations. Tests were only performed in simplified motions of pure scapular abduction or

flexion, whereas most daily activities have ranges of motion that combine abduction and flexion with obligate rotations ²⁰. Moreover, the model is based on a range of subjects with normal anatomy, and this study varied the CSA in isolation, whereas there might be other changes present with a change in CSA angle, such as glenoid version or muscle stiffness that may influence the model outputs. Additionally, a change in anatomy might also result in a further change in kinematics, although this was mitigated in this study by using a set of data from six healthy subjects, rather than just from one subject. Finally, we could have studied the different components of the CSA separately but even if the lateral acromial roof extension has a greater influence in pathogenesis of degenerative RCT and concentric OA than acromial height or glenoid inclination, the CSA remain the best factor to predict these pathologies ⁶.

Conclusion

Through a validated computational shoulder model, combined with in vivo motion analysis experiments, this study demonstrates that changes in the CSA modify GHJ biomechanics. Increasing the CSA results in higher shear forces, requiring increased rotator cuff use to neutralize the shear which is potentially damaging in the long term. Decreasing the CSA results in a higher joint compressive force which leads to increased joint wear.

These findings support previous clinical observational and biomechanical studies that alterations in CSA may have a role in common shoulder pathologies such RCT or OA.

Consequently, surgical restoration to a "normal" CSA is recommended when treating patients with such pathologies, for example, lateral acromioplasty after rotator cuff repair or ensuring control of glenoid inclination when conducting arthroplasty surgery.

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reporting of human joint motion--Part II: shoulder, elbow, wrist and hand. J. Biomech. 338 2005 May;38(5):981–992. https://doi.org/10.1016/j.jbiomech.2004.05.042 339 340 Figure 1. **Illustration of the UKSNM.** 341 342 Figure 2. Statistically significant changes in joint forces due to changed CSA. These 343 conditions that showed a main effect in the ANOVA analysis. The error bars indicate standard 344 345 deviation. 346 347 Figure 3. Vector plot of the maximum joint reaction forces in the medio-lateral and superiorinferior direction for the three CSA angles. The integrated shear force in the superior-inferior 348 direction (SI) was significantly larger for increased CSA compared to normal CSA. The 349 reduced CSA showed significantly higher compressive forces (CF) compared to normal CSA 350 and increased CSA. 351 352 Table 1. Repeated measures ANOVA. Shown are the main effects for the separate force 353 directions (AP, SI, CF), and the pairwise comparisons for the force directions that 354 significantly differed between CSA conditions. Nor = Normal CSA (33°), Red = Reduced 355 CSA (28°), Inc = Increased CSA (38°). 356 357

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Table 1. Repeated measures ANOVA. Shown are the main effects for the separate force directions (AP, SI, CF), and the pairwise comparisons for the force directions that significantly differed between CSA conditions. Nor = Normal CSA (33°) , Red = Reduced CSA (28°) , Inc = Increased CSA (38°) .

Variable	Mauchly's	Main effect		Pairwise		
	sphericity			CSA		
				Nor-Red	Nor- Inc	Red- Inc
integrated AP shear	$\chi^2(2)=9.5$,	p = 0.598				
	p<.01, ϵ =.52					
max AP shear	$\chi^2(2)=11.6$,	p = 0.595				
	p<.01, ε =.51					
integrated SI shear		p = 0.026	F(2,10) = 5.34		p = 0.044	
max SI shear	$\chi^2(2)=[],$	p = 0.068				
	p<.05, ϵ =.55					
integrated CF	$\chi^2(2)=6.23$,	$\mathbf{p} = 0.003$	F(1.1, 5.6)=24.55	p = 0.001		p = 0.01
	p<.05, ϵ =.56					
max CF	$\chi^2(2)=6.84$,	p = 0.009	F (2,10) =14.97	p = 0.008		p = 0.03
	p<.05, ϵ =.55					





