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Sulfur Scavenging in a Mesoscale Model With Quasi-Spectral Microphysics: Two-Dimensional Results for Continental and Maritime Clouds

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A three-dimensional mesoscale numerical model (Nickerson et al., 1986) with quasi-spectral microphysics has been extended to include gas and aerosol removal by cloud droplets and raindrops. Combining meteorological predictions and pollutant scavenging parameterizations, two-dimensional sensitivity tests have been carried out for continental and maritime clouds over an idealized topography. Nucleation scavenging is the most efficient in-cloud removal mechanism; however, differences in cloud droplet spectra between continental and maritime clouds lead to differences in their scavenging efficiencies for gases and aerosols, thereby emphasizing the need for the simultaneous treatment of meteorological and physicochemical processes.

1. INTRODUCTION

Wet deposition is the result of complex nonlinear interactions between meteorological and physicochemical factors. Identification and knowledge of those interactive processes have been significantly improved in recent years as a result of field investigations, laboratory studies, and theory aided by numerical simulations. Some numerical studies [Hegg et al., 1984b; Tremblay and Leighton, 1984; Kitada et al., 1984] concentrate on the redistribution of trace gases and aerosols by various precipitating cloud systems. In such models, meteorological fields are usually prespecified under the assumption of steady airflows [Tremblay and Leighton, 1984] or by objective analysis of the wind field [Kitada et al., 1984]. Moreover, cloud microphysics is only grossly parameterized, thus excluding any explicit calculation of the scavenging rates [Hegg et al., 1984b], since nucleation and capture rates are strongly dependent on hydrometeor and aerosol spectra.

The aim of this paper is to exemplify the usefulness of a quasi-spectral parameterization of liquid water and aerosols so as to describe nucleation scavenging and SO₂ dissolution into cloud droplets. A microphysical scheme, with raindrop spectra only, has already been incorporated into a three-dimensional mesoscale model [Nickerson et al., 1986] for simulating precipitation. Here we present an extended microphysical version of this scheme allowing for an improved explicit representation of the condensation/evaporation processes. Two-dimensional simulations are next performed to evaluate the relative contributions of each scavenging process in typical continental and maritime clouds.

2. MODEL PRESENTATION

2.1. Description of Meteorological Model

The three-dimensional hydrostatic mesoscale model is based upon primitive equation resolution. The horizontal grid length is typically 10 km and the time step is 10 s. There are 15 computational levels in the vertical, equally spaced in a

terrain-following (*nu*) coordinate system. A centered leap-frog scheme is used with an Asselin [1972] filter. Lateral boundary conditions are of the Orlanski [1976] type for the normal velocity component. The tangential velocity and all other prognostic variables are computed using advective conditions on outflow boundaries and prescribed values at inflow points. A viscous damping layer at the top of the domain [Klemp and Lilly, 1978] is used to absorb vertically propagating waves. A comprehensive description of the dynamical computations of the model can be found in the work by Nickerson et al. [1986].

The prognostic variables in the warm-rain version of the model are ground pressure Π , horizontal wind (u , v), vapor mixing ratio q_v , and potential temperature Θ . Here Θ is predicted in flux form as

$$\frac{\partial(\Pi\Theta)}{\partial t} = -\frac{\partial}{\partial x}(\Theta\Pi u) - \frac{\partial}{\partial y}(\Theta\Pi v) - \frac{\Pi}{\sigma'} \frac{\partial}{\partial v}(\sigma'\Theta v) + \frac{L_v\Pi}{C_{pm}\bar{p}} \frac{\partial q_v}{\partial t} \Big|_{\text{condensation}} + F_{\Theta} \quad (1)$$

Predictions are made of both rainwater mixing ratio q_{rw} and total number concentration N_{rw} , assuming a lognormal drop distribution. Extensive use of Berry and Reinhardt's [1973] formulation has been made for parameterization of the auto-conversion, accretion, and self-collection processes. For further details, the reader is referred to Nickerson et al. [1986].

Cloud droplets are also assumed to be lognormally distributed. In the diameter range D to $D + dD$, the cloud droplet concentration is given by

$$dN_{cw} = \frac{N_{cw}}{(2\pi)^{1/2}\sigma_c D} \exp\left(-\frac{1}{2\sigma_c^2} \ln^2 \frac{D}{D_{c_0}}\right) dD \quad (2)$$

where N_{cw} is the total number concentration of droplets; D_{c_0} , the modal diameter; and σ_c , the dispersion parameter. Integration of (2) over the entire droplet spectrum yields the following expression for q_{cw} , the cloud water mixing ratio:

$$q_{cw} = \frac{N_{cw}}{\rho_a} \left(\frac{\pi}{6} D_{c_0}^3 \rho_w\right) \exp\left(\frac{9}{2} \sigma_c^2\right) \quad (3)$$

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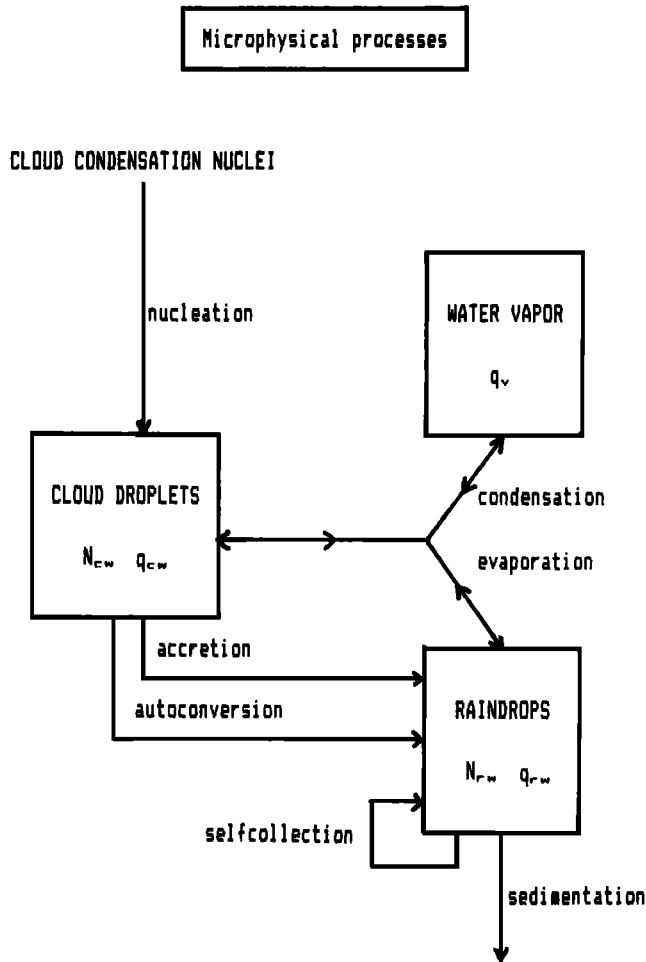


Fig. 1. Synopsis of the microphysical processes in the mesoscale model.

where ρ_a and ρ_w are the densities of air and liquid water, respectively. To close the system of (2) and (3), σ_c is assumed constant, equal to 0.15 (continental case) or to 0.28 (maritime case). Those values are taken from *Berry and Reinhardt* [1973], where σ_c is deduced from the expression of the relative variance of the cloud droplet spectrum number density function. Predicting N_{cw} and q_{cw} , as for the rainwater, D_{c0} is then computed from (3).

The microphysical processes to be considered are schematically depicted in Figure 1. The number of condensation nuclei active at supersaturation S , is given by

$$N = CS^k \quad (4)$$

where C and k are empirical constants. For continental clouds, C is set to 3500 cm^{-3} and k to 0.9, while for maritime clouds $C = 100$ and $k = 0.7$. These experimental values have been adopted as being typical of maritime and continental clouds in different parts of the world [*Pruppacher and Klett*, 1978].

From (4) the number of cloud condensation nuclei activated per second is derived. It is equal to the time change of the number of cloud droplets formed through heterogeneous nucleation. It is not possible to calculate this number directly, since the time constant of the equation for dS/dt can be less than 0.1 s and so is much smaller than the time step of the model, $\Delta t = 10$ s. Following *Twomey* [1959], an upper bound

for the supersaturation S_{\max} is calculated which gives the maximum number of activated nuclei and the number of cloud droplets formed through nucleation during every time step. This calculation is quite similar to the one reported by *Pruppacher and Klett* [1978]:

$$S \leq \left\{ \frac{\rho_a [A_1 (dP/dt)]^{3/2}}{2\pi\rho_w k C A_2 A_3^{3/2} \beta[(k/2), (3/2)]} \right\}^{1/(k+2)} \quad (5)$$

where

$$A_1 = \frac{1}{P} - \frac{\varepsilon L_v}{RT^2 \rho_a C_p}$$

$$A_2 = \frac{1}{q_{vs}} + \frac{\varepsilon L_v^2}{RT^2 C_p}$$

and

$$A_3 = \frac{L_v \rho_w}{KT} \left(\frac{L_v}{R_w T} - 1 \right) + \frac{\rho_w R_w T}{e_{sw}(T) D_v}$$

Symbols and units are given in the appendix.

The nucleation term is finally taken into account by adding to the predicted value of N_{cw} the term N_{nuc} , given by

$$N_{\text{nuc}} = \max(CS_{\max}^k - N_{cw\text{-total}}, 0) \quad (6)$$

where $N_{cw\text{-total}}$ is the total number of cloud droplets already formed through nucleation. If cloud condensation nuclei have been activated, the newly nucleated cloud droplets have a critical diameter corresponding to the maximum of the supersaturation S_{\max} , namely:

$$D_{\text{crit}} = (4M_w \sigma_w) / (3S_{\max} T R \rho_w) \quad (7)$$

The corresponding change in mixing ratio q_{nuc} is deduced from N_{nuc} :

$$q_{\text{nuc}} = \frac{\pi}{6} \frac{\rho_w}{\rho_a} D_{\text{crit}}^3 N_{\text{nuc}} \quad (8)$$

Newly nucleated droplets will in fact grow to a size larger than D_{crit} over the 10-s time step, therefore (8) is a lower limit for the change in mixing ratio.

The condensation/evaporation term appears in the latent heat release term (equation (1)) and in the prediction equations for the mixing ratios q_v , q_{cw} , and q_{rw} , according to the following relationship:

$$\left. \frac{\partial q_v}{\partial t} \right|_{\text{condensation/evaporation}} = - \left. \frac{\partial q_{cw}}{\partial t} \right|_{\text{condensation/evaporation}} - \left. \frac{\partial q_{rw}}{\partial t} \right|_{\text{condensation/evaporation}} \quad (9)$$

In order to obtain the rate of change of q_{cw} and q_{rw} , integration is made over the cloud droplet and raindrop spectra. Calculations are performed first for q_{cw} . The rate of change of q_{cw} is expressed by

$$\frac{\partial q_{cw}}{\partial t} = \frac{\rho_w}{\rho_a} \int_0^\infty \frac{\pi}{2} D^2 \frac{dD}{dt} \frac{N_{cw}}{(2\pi)^{1/2} \sigma_c D} \exp\left(-\frac{1}{2\sigma_c^2} \ln^2 \frac{D}{D_{c0}}\right) dD \quad (10)$$

Then, the time rate of change for diameter D of cloud droplets due to condensation or evaporation is

$$\frac{dD}{dt} = \frac{A_3 S}{D} \quad (11)$$

where A_3 is the thermodynamical function in (5). This leads to

$$\left. \frac{\partial q_{cw}}{\partial t} \right|_{\substack{\text{condensation} \\ \text{evaporation}}} = \frac{\rho_w}{\rho_a} \frac{\pi}{2} A_3 S N_{cw} D_{c_0} \exp \frac{\sigma_c^2}{2} \quad (12)$$

A similar expression is calculated for

$$\left. \frac{\partial q_{rw}}{\partial t} \right|_{\substack{\text{condensation} \\ \text{evaporation}}}$$

apart from the fact that a ventilation factor arises for the time rate of change of raindrop diameter:

$$\frac{dD_r}{dt} = \frac{A_3 S \bar{f}}{D_r} \quad (13)$$

After Pruppacher and Rasmussen [1979], \bar{f} is parameterized by

$$\bar{f} = 0.78 + 0.308X \quad (14)$$

where $X = Re^{1/2} Sc^{1/3}$.

Then, we have adjusted the variable X as a function of diameter D_r by

$$X = -1.406 \times 10^6 D^2 + 1.725 \times 10^4 D - 0.675 \quad (15)$$

Replacing dD_r/dt by its expression as a function of D_r and after integration over the raindrop spectrum, the rate of change of q_{rw} is written as

$$\left. \frac{\partial q_{rw}}{\partial t} \right|_{\substack{\text{condensation} \\ \text{evaporation}}} = \frac{\rho_w}{\rho_a} \frac{\pi}{2} A_3 S N_{rw} [0.572 D_{r_0} \exp(\sigma_r^2/2) + 5.31 \times 10^3 D_{r_0}^3 \exp(2\sigma_r^2) - 4.33 \times 10^5 D_{r_0}^3 \exp(\frac{9}{2}\sigma_r^2)] \quad (16)$$

Because of the discrepancy between the model time step and the supersaturation time constant, it is not possible to calculate S exactly in (12) and (16). The scheme of Sakakibara [1979] is used here, because it is adapted for stable computation of the condensation process with a large time step of the order of 10 s. The method consists in solving analytically the following equation:

$$\frac{dS}{dt} = (C_1 + C_2 + C_3)S + C_3 \quad (17)$$

where:

$$C_1 = -\frac{1}{q_{vs}} \frac{\rho_w}{\rho_a} \frac{\pi}{2} A_3 S \Sigma \quad (18)$$

$$C_2 = -\frac{\varepsilon L_v^2}{RT^2 C_p} \frac{\rho_w}{\rho_a} \frac{\pi}{2} A_3 S \Sigma \quad (19)$$

$$C_3 = \left(\frac{1}{P} - \frac{\varepsilon L_v}{RT^2 \rho_a C_p} \right) \frac{dP}{dt} \quad (20)$$

and

$$\Sigma = N_{cw} D_{c_0} \exp(\sigma_c^2/2) + N_{rw} [0.572 D_{r_0} \exp(\sigma_r^2/2) + 5.31 \times 10^3 D_{r_0}^3 \exp(2\sigma_r^2) - 4.33 \times 10^5 D_{r_0}^3 \exp(\frac{9}{2}\sigma_r^2)] \quad (21)$$

An approximate average value \bar{S} over the time interval Δt is then evaluated as

$$\bar{S} = -\frac{C_3}{C} - \left(S_0 + \frac{C_3}{C} \right) \left(1 - \frac{\exp(C\Delta t)}{C\Delta t} \right) \quad (22)$$

where $S_0 (= q_v/q_{vs} - 1)$ is the supersaturation at the beginning of the time step Δt and $C = C_1 + C_2 + C_3$. This value \bar{S} is used in (12) and (16). The rate of change of q_v is

$$\left. \frac{\partial q_v}{\partial t} \right|_{\substack{\text{condensation} \\ \text{evaporation}}} = -\frac{\rho_w}{\rho_a} \frac{\pi}{2} A_3 \bar{S} \Sigma \quad (23)$$

With evaporation the smallest drops of the spectrum can disappear entirely. This explains the sink terms in the equation used for N_{cw} and N_{rw} prediction in case of total evaporation. The term

$$\left. \frac{\partial N_{cw}}{\partial t} \right|_{\text{evaporation}}$$

is calculated as in the work by Nickerson et al. and the same expression is used for

$$\left. \frac{\partial N_{rw}}{\partial t} \right|_{\text{evaporation}}$$

Based upon a simplified evaluation of supersaturation, these parameterizations for the nucleation and the condensation/evaporation processes allow for explicit calculations of aerosol nucleation rates and dissolution rates of gases in the aqueous phase. This is very important, since these two processes are admittedly the most efficient among the various pollutant scavenging processes in the troposphere [Garland, 1978]. Another advantage of this quasi-spectral formulation of cloud water is that it allows for a detailed description of three regimes of aerosol capture by raindrops.

2.2. Aerosol and Gas Scavenging Parameterizations

As for the hydrometeors, aerosol particles are assumed to be lognormally distributed, the dispersion parameter being set to $\ln 2$ [Dana and Hales, 1976]. One discriminates between three categories of particles: those free in the air and others attached to cloud droplets or raindrops, respectively. Only sulfate particles are considered here. An overview of the physicochemical processes is given in Figure 2. Sulfate volume mixing ratio in cloud and rainwater can be increased through conversion of dissolved SO_2 . Separate prognostic equations are written for each sulfate category for both number concentration and volume mixing ratio. These are listed below:

$$\frac{\partial \Pi C_{ap}}{\partial t} = -A(C_{ap}) - \Pi \left(\left. \frac{\partial C_{ap}}{\partial t} \right|_{\text{Brownian diffusion}} + \left. \frac{\partial C_{ap}}{\partial t} \right|_{\text{dynamical capture}} \right) + F_{C_{ap}} \quad (24)$$

$$\frac{\partial \Pi q_{ap}}{\partial t} = -A(q_{ap}) - \Pi \left(\left. \frac{\partial q_{ap}}{\partial t} \right|_{\text{Brownian diffusion}} + \left. \frac{\partial q_{ap}}{\partial t} \right|_{\text{dynamical capture}} \right) + F_{q_{ap}} \quad (25)$$

$$\frac{\partial \Pi C_{cp}}{\partial t} = -A(C_{cp}) + \Pi \left(\left. \frac{\partial C_{ap}}{\partial t} \right|_{\text{Brownian diffusion}} - \left. \frac{\partial C_{cp}}{\partial t} \right|_{\text{accretion}} - \left. \frac{\partial C_{cp}}{\partial t} \right|_{\text{autoconversion}} \right) + F_{C_{cp}} \quad (26)$$

$$\frac{\partial \Pi q_{cp}}{\partial t} = -A(q_{cp}) + \Pi \left(\left. \frac{\partial q_{ap}}{\partial t} \right|_{\text{Brownian diffusion}} - \left. \frac{\partial q_{cp}}{\partial t} \right|_{\text{accretion}} - \left. \frac{\partial q_{cp}}{\partial t} \right|_{\text{autoconversion}} + \frac{3}{2} \rho_a \left. \frac{\partial q_{ds}}{\partial t} \right|_{\text{oxidation}} \right) + F_{q_{cp}} \quad (27)$$

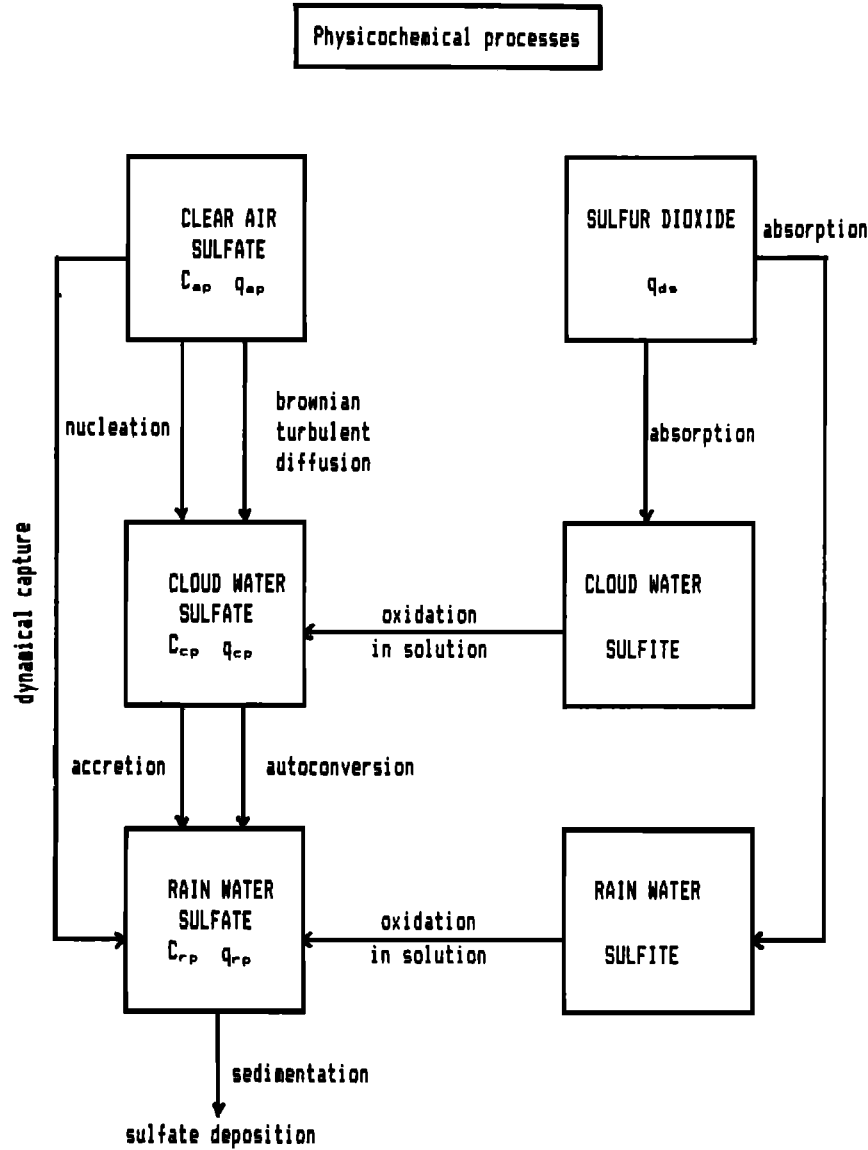


Fig. 2. Synopsis of the physicochemical processes in the mesoscale model.

$$\frac{\partial \Pi C_{rp}}{\partial t} = -A(C_{rp}) + \Pi \left(\left. \frac{\partial C_{ap}}{\partial t} \right|_{\text{dynamical capture}} + \left. \frac{\partial C_{cp}}{\partial t} \right|_{\text{accretion}} + \left. \frac{\partial C_{cp}}{\partial t} \right|_{\text{autoconversion}} + \left. \frac{\partial C_{rp}}{\partial t} \right|_{\text{sedimentation}} \right) + F_{C_{rp}} \quad (28)$$

$$\frac{\partial \Pi q_{rp}}{\partial t} = -A(q_{rp}) + \Pi \left(\left. \frac{\partial q_{ap}}{\partial t} \right|_{\text{dynamical capture}} + \left. \frac{\partial q_{cp}}{\partial t} \right|_{\text{accretion}} + \left. \frac{\partial q_{cp}}{\partial t} \right|_{\text{autoconversion}} + \left. \frac{\partial q_{rp}}{\partial t} \right|_{\text{sedimentation}} + \frac{3}{2} \rho_a \left. \frac{\partial q_{ds}}{\partial t} \right|_{\text{oxidation}} \right) + F_{q_{rp}} \quad (29)$$

where the operator A applied to a variable q is defined as

$$A(q) = \frac{\partial}{\partial x} (q \Pi u) + \frac{\partial}{\partial y} (q \Pi v) + \frac{\Pi}{\sigma'} \frac{\partial}{\partial v} (\sigma' q v)$$

The last terms F in (24)–(29) are the friction terms. Each friction term consists, in a vertical eddy diffusion term repre-

senting the turbulent transport of a variable within the planetary boundary layer [Nickerson, 1979] and in a horizontal diffusion term, of the form:

$$\pi K_H \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)$$

operating on a v -surface.

Aerosol scavenging by hydrometeors occurs through two different mechanisms. First, aerosols are scavenged through direct capture by raindrops: the associated capture rate is calculated after Dana and Hales [1976]. Second, indirect scavenging can take place through a two-stage process [Pruppacher and Klett, 1978]. In the first stage, most aerosols are incorporated into cloud water by nucleation and by Brownian and turbulent diffusion. In the second stage this polluted cloud water is accreted by falling raindrops or cloud droplets to form larger raindrops. The parameterizations developed for Brownian and turbulent diffusion rates are from Dingle and Lee [1973]. A comprehensive survey for removal rate parameterizations can be found in the work by Chaumerliac et al. [1986].

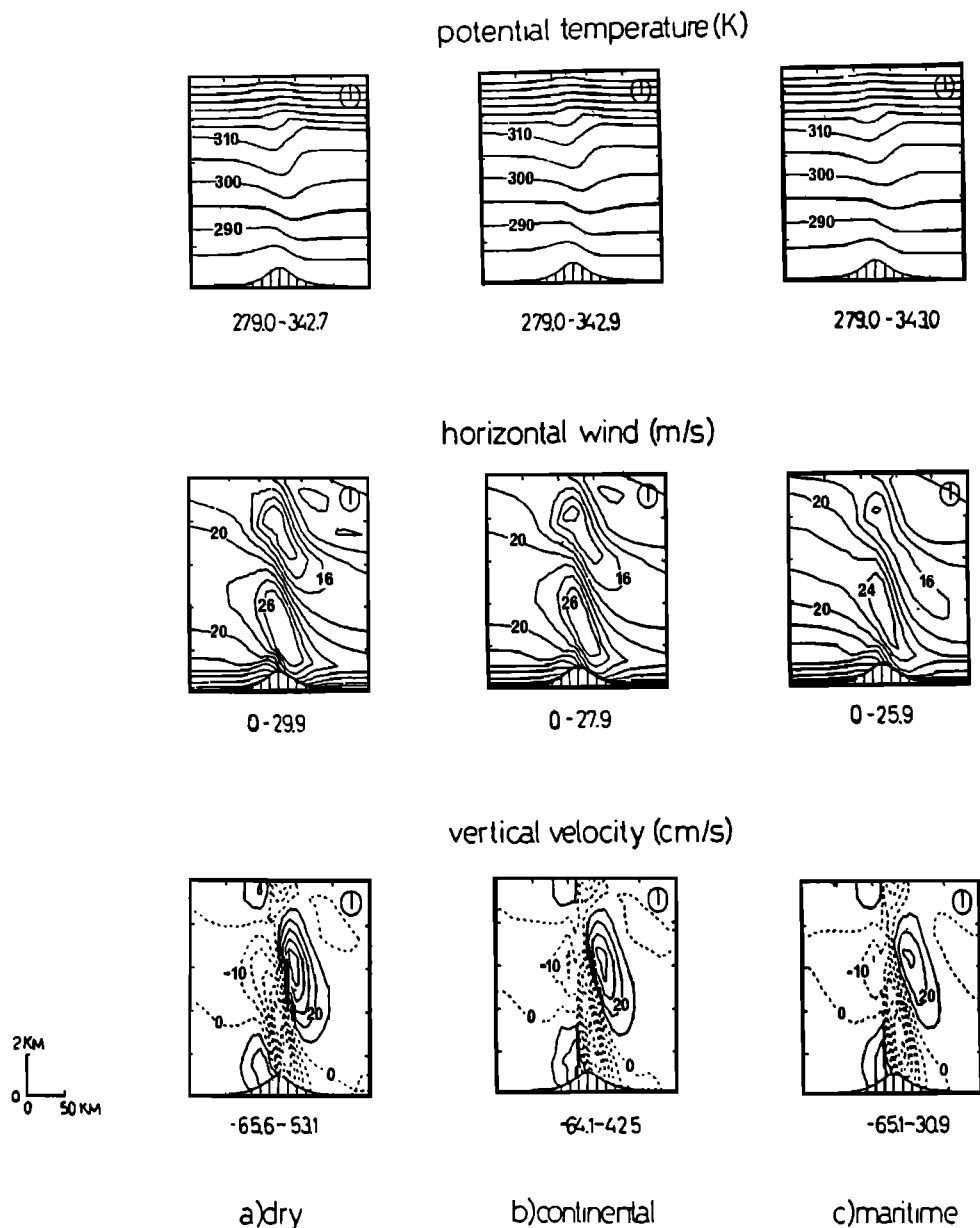


Fig. 3. Potential temperature, horizontal and vertical velocities for (a) dry, (b) continental, and (c) maritime cases in the presence of orography. Extreme values of the isocontours are indicated at the bottom of each figure.

The rates of accretion and autoconversion, for the transfer of cloud water sulfates to rainwater sulfates, are calculated using the microphysical rates with proportionality relationships.

The sedimentation term is formulated as follows:

$$\left. \frac{\partial C_{rp}}{\partial t} \right|_{\text{sedimentation}} = \frac{\partial}{\partial z} \left(\frac{C_{rp}}{N_{rw}} S_n \right) \quad (30)$$

where S_n is the sedimentation flux of raindrops. The term

$$\left. \frac{\partial q_{rp}}{\partial t} \right|_{\text{sedimentation}}$$

is formally similar.

The nucleation rates, not appearing in the set of equations (24)–(29) are subtracted from C_{ap} and q_{ap} and added to C_{cp} and q_{cp} after every advance in time. The term C_{ap-nuc} is proportional to N_{nuc} but the term q_{ap-nuc} has to be calculated by

$$q_{ap-nuc} = \frac{4}{3} \pi r_{nuc}^3 C_{ap-nuc} \quad (31)$$

The dry condensation nucleus radius r_{nuc} is required and is calculated by equating [Prodi and Tampieri, 1982]:

$$S_{max} \approx \frac{8(2\pi)^{1/2}}{9\rho_w} \left(\frac{\sigma m_w}{RT} \right)^{3/2} \left(\frac{imm_w}{m_N} \right)^{-1/2} \quad (32)$$

The nucleus mass m , then the dry radius r_{nuc} are deduced from this relationship.

Considering now gaseous pollutants, prediction is made of the SO_2 mixing ratio. Sulfur dioxide is absorbed by cloud droplets and raindrops before being oxidized in solution. Only major SO_2 oxidants in aqueous phase, ozone, and hydrogen peroxide are considered here. The formulations of SO_2 dissolution and its subsequent oxidation are derived from Hegg *et al.* [1984b]. O_3 and H_2O_2 are 50 ppb and 1 ppb, respectively, initially in the gas phase and the rates of oxidation of S(IV) are based on Maahs [1983] for O_3 and on Martin [1984] for H_2O_2 .

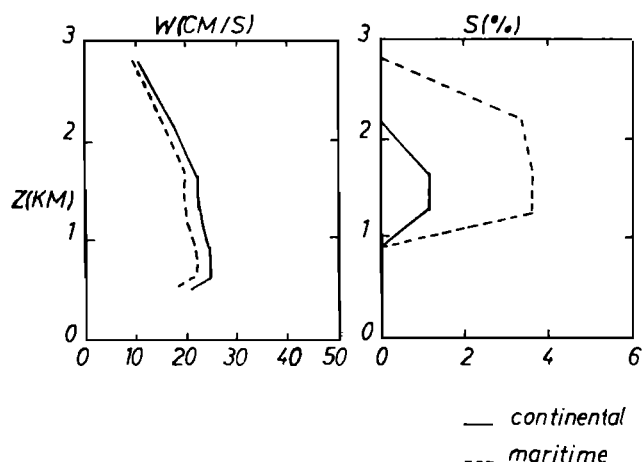


Fig. 4. Vertical profiles of vertical velocity and supersaturation for continental clouds (solid lines) and maritime clouds (dashed lines) at $x = 110$ km.

3. MODEL RESULTS

3.1. Initial Conditions

In order to test simultaneously the microphysical and physicochemical parameterizations, a series of two-dimensional sensitivity tests were carried out. This choice has been made because two-dimensional simulations are less time consuming than three-dimensional ones and because such idealized tests are well documented as regards to the dynamics [Klemp and Lilly, 1978; Mahrer and Pielke, 1978]. Comparative tests between dry, continental, and maritime conditions have been performed. Because of complex interactions between meteorological and physicochemical processes, such tests are especially useful for identifying the relative contributions of each mechanism.

The model is run over an idealized bell-shaped mountain, 1 km high and 25 km in halfwidth. A two-layer atmosphere is considered, with a lower layer of constant lapse rate up to 8 km and an isothermal layer aloft. The initial horizontal wind speed is uniformly 20 ms^{-1} and the relative humidity is 80% below 3 km.

In addition, the SO_2 and sulfate variables are initialized with the following exponential profiles [Hegg et al., 1984b]:

$$q_{ds}(z) = 4.3 \times 10^{-9} \exp(-z/2000) \quad (33)$$

$$q_{ap}(z) = 4 \times 10^{-12} \exp(-z/3500) \quad (34)$$

$$C_{ap}(z) = 10^9 \exp(-z/3500) \quad (35)$$

where z is the altitude, all units being in MKS.

Our selected case is typical of background pollution in Western Europe [Georgii, 1978; Georgii and Meixner, 1980]. Tests to evaluate interactions between microphysical and physicochemical processes together with comparisons between continental and maritime cases are performed over 6-hour simulation periods. In the comparison between continental and maritime clouds, one discriminates between their dynamical features, their spectra, and the relative efficiency with which they can scavenge aerosols and gases.

3.2. Meteorological Fields

First, the dynamics of mountain waves are investigated under three cases: dry case (no moisture) as opposed to conti-

mental and maritime clouds. Figure 3a displays the results of a dry simulation, while Figures 3b and 3c refer to simulations for continental and maritime cases, respectively. When comparing Figure 3a and Figures 3b and 3c, one can observe that moist waves are weaker in amplitude than dry waves [Durran and Klemp, 1983]. Between Figures 3b and 3c, noticeable differences appear in the dynamical fields, with larger vertical velocities in the continental case. This is even more obvious for the vertical profiles in Figure 4 where vertical velocities are drawn as a function of height at a selected grid point (one grid point upwind from the mountain top). Vertical supersaturation profiles are reported in Figure 4. We find that supersaturations in the region of active updrafts are about twice as great in the maritime case as in the continental one. Profiles in Figure 4 are quite comparable to the results of Lee and Pruppacher [1977], in their comparative study of continental and maritime cumuli within the dynamical framework of an entraining air parcel.

In addition to changes in dynamical features, other typical differences between continental and maritime clouds can be found in their spectra, determined from the cloud condensation nuclei spectra. Thus high droplet concentrations ($500\text{--}600 \text{ cm}^{-3}$) with narrow spectra centered at about $10 \mu\text{m}$, typical of continental clouds have been obtained. The maritime cloud simulated in the model contains about 50 droplets cm^{-3} with diameter of about $25 \mu\text{m}$. In Figure 5, vertical cross sections of cloud water and rainwater mixing ratios are displayed which reflect the major differences between continental and maritime clouds. Cloud water contents are about twice as large in the continental case, while rainwater contents are considerably larger in the maritime case. Consequently, after 6 hours of model time, one observes in Figure 6 that the maritime cloud rains about 10 times more than the continental cloud and that the maximum of precipitation is not located at the same position in the continental and maritime cases. In Figure 6 there is a slight shift of both the maxima of precipitation, the continental cloud raining farther from the mountain top than the maritime cloud. This is probably due to continental small cloud droplets being more sensitive to advection leading to longer growth times before effective production of rain by coalescence [Squires, 1958].

3.3. Aerosol Scavenging Results

Nucleation is widely recognized as the most efficient process among all scavenging mechanisms [Flossmann et al., 1985; Jensen and Charlson, 1984; Radke, 1983; Hegg et al., 1984a]. In order to evaluate the effects of nucleation scavenging, we proceed to two sensitivity tests. In the first run all the scavenging processes are considered, while in the second run the nucleation scavenging term is set equal to zero. These two cases (with and without nucleation) are considered for both maritime and continental clouds. To study the relative efficiency of aerosol scavenging in the two types of clouds, the same initial aerosol distribution is assumed. This vertical profile, typical of continental cases has been specified earlier (see section 3.1, (equations (34)–(35))).

Results are presented in Figures 7 and 8 in the form of vertical cross sections for concentrations of aerosols attached to cloud droplets (Figure 7) and aerosols removed by rain (Figure 8) after a 6-hour run. A large difference in the number of aerosols collected by cloud water is observed between the run accounting only for the dynamical capture of aerosols

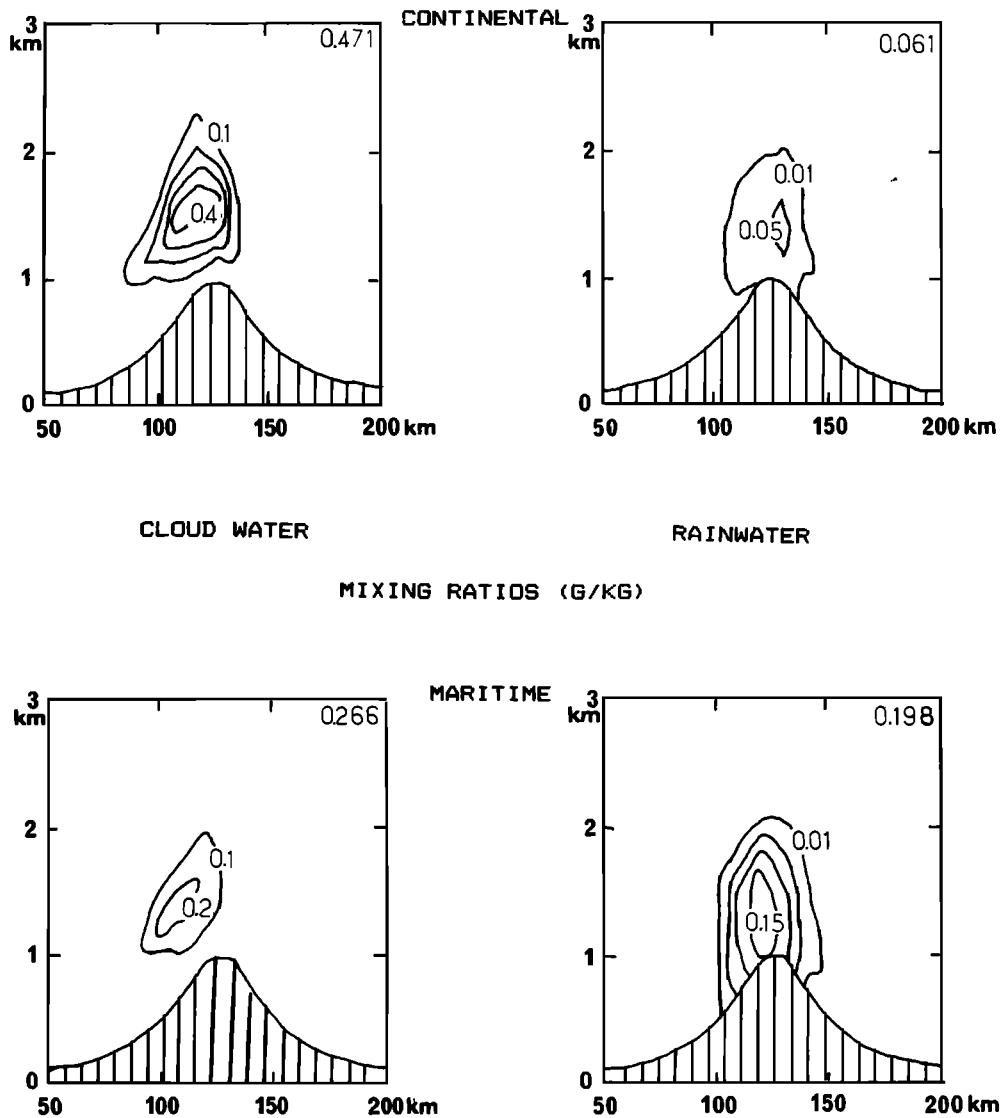


Fig. 5. Vertical cross sections of (a) cloud water mixing ratio and (b) rain water mixing ratio after 6-hour model time in continental and maritime cases. The maxima values of q_{cw} and q_{rw} are reported in the right corner of each figure.

(Figure 7a) and the run including all the scavenging processes (Figure 7b). There is 1–2 orders of magnitude difference between the results of the simulations with and without nucleation in continental and maritime cases, respectively. The continental cloud is more efficient for in-cloud scavenging (Figure 7) and the contribution of scavenging by Brownian and turbulent diffusion (Figure 7a) is not completely negligible for small cloud droplets which are apt to collect aerosols of radii less than $0.1 \mu\text{m}$. This has already been suggested by Garland [1978]. On the contrary, maritime clouds are much more efficient for removing aerosols (Figure 8), even when the nucleation term has been omitted (Figure 8a). This is essentially due to the predominance of autoconversion in the initiation of the rain process in maritime conditions. As already underlined, it can be inferred that sulfate wet deposition will be more effective in the case of maritime cloud. This will be discussed later, in section 3.5.

3.4. Gas Scavenging Results

Before studying sulfate deposition, SO_2 dissolution and oxidation by H_2O_2 and O_3 and its subsequent transformation to sulfates must be considered.

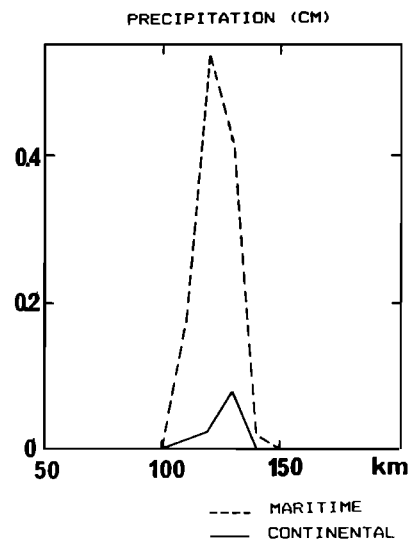


Fig. 6. Precipitation amount (in centimeters) cumulated over a 6-hour period for continental (solid line) and maritime clouds (dashed line).

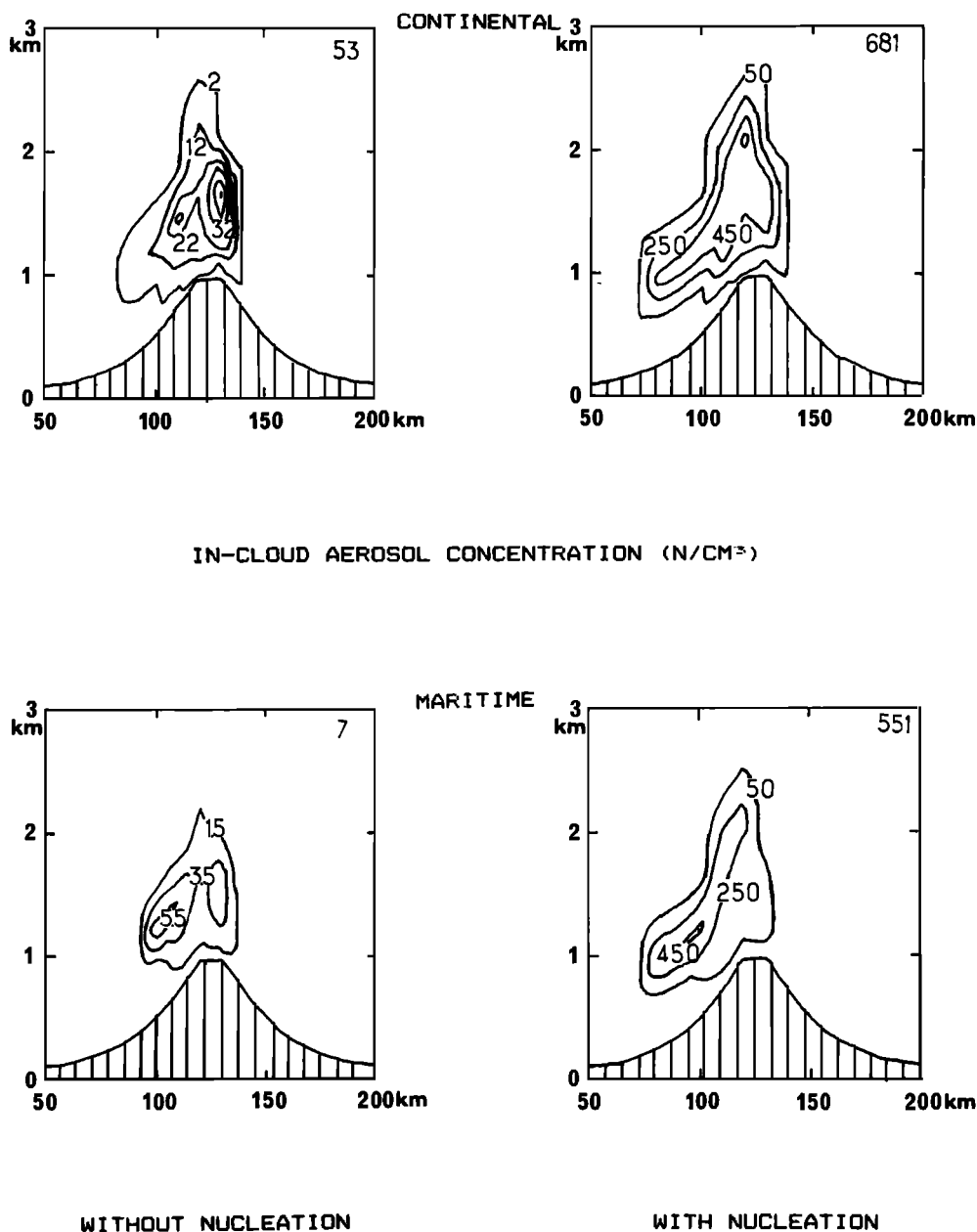


Fig. 7. Vertical cross sections of in-cloud aerosol concentration C_{cp} (in number per cubic centimeter) in continental and maritime clouds (a) without nucleation and (b) with nucleation. The maximum value of C_{cp} is reported in the right corner of each figure.

Results of sensitivity tests are first presented in order to study the relative impact of O_3 and H_2O_2 oxidation on the conversion of SO_2 into sulfate particles. Vertical cross sections of SO_2 mixing ratio after oxidation by ozone (Figure 9a) and after oxidation by both O_3 and H_2O_2 (Figure 9b) have been superimposed on vertical cross sections, for which only advection effects have been considered (dashed isocontours in Figure 9). Clear SO_2 depletion coinciding with the presence of cloud (shaded zones) is observed in Figure 9 when oxidation occurs. The reduction in SO_2 mixing ratio is even greater when considering simultaneous oxidation by O_3 and H_2O_2 (Figure 9b) than when considering oxidation by O_3 only (Figure 9a). If we now focus (Figure 10) on the time evolution of SO_2 mixing ratio, the oxidation by H_2O_2 appears to occur quite rapidly (after about half an hour model time), after which slower oxidation by O_3 takes place for several hours.

Oxidation by H_2O_2 is initially fast and leads to a rapid decrease in cloud water pH; however, it cannot be sustained past the first few minutes of cloud because of H_2O_2 depletion. The pH was initially set to 5; it falls down to a value less than 4. When only oxidation by O_3 occurs, the pH is not very much affected and differences between curves 2 and 3 in Figure 10 can be explained by the fact that O_3 contribution to sulfate formation is more efficient when the pH is greater than 4 [Hoffmann and Jacob, 1984; Seigneur and Saxena, 1984].

Surprisingly, we did not find any striking difference between maritime and continental clouds as regards the SO_2 mixing ratios after oxidation in the aqueous phase. Presumably, some compensating effect arises between the dynamical and physicochemical processes leading to such a similarity. In order to identify which ones of those processes are balancing each other we first try to switch off dynamical/microphysical inter-

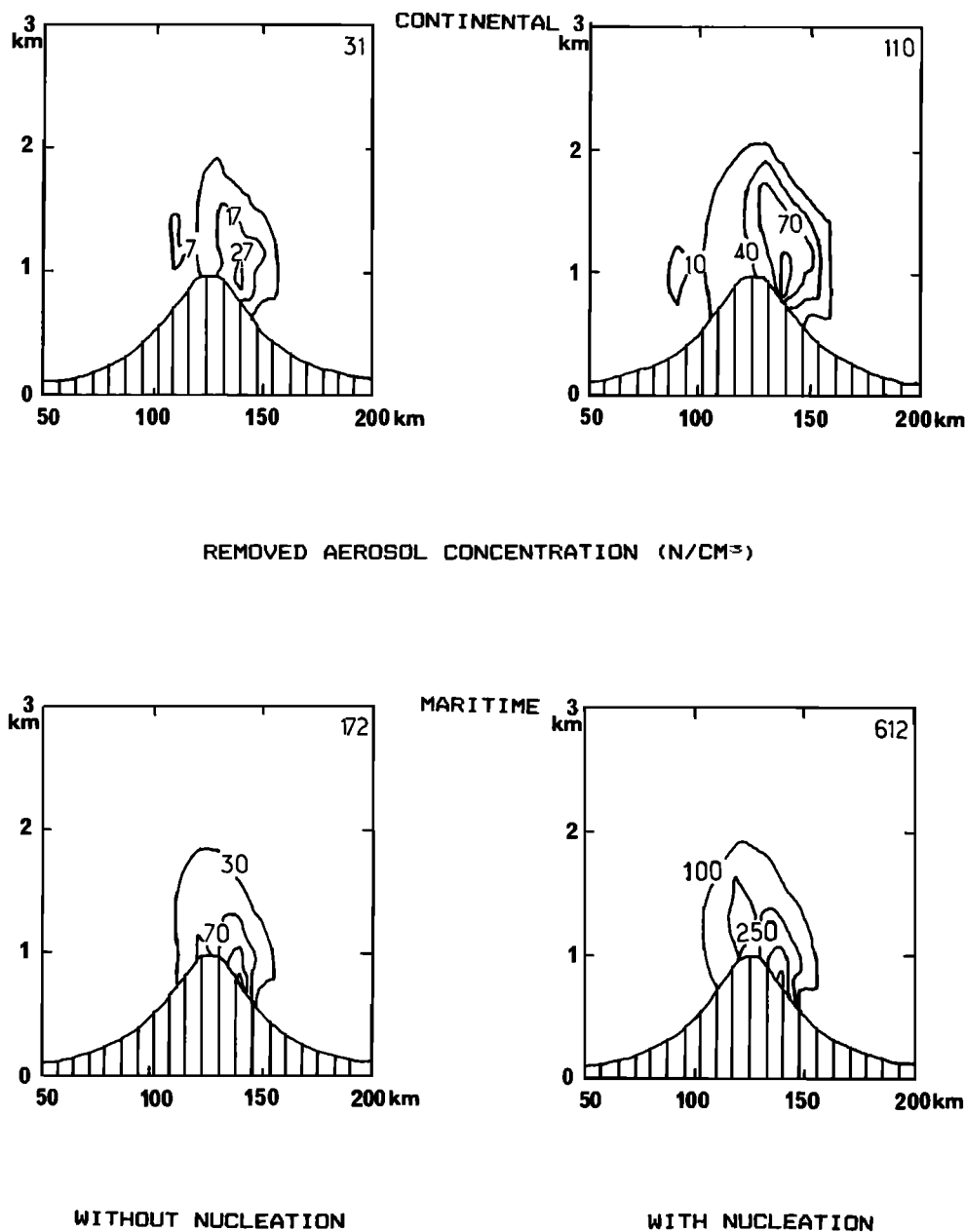


Fig. 8. Same as Figure 7, but for removed aerosol concentration C_{rp} .

actions in the model by setting to zero the term of latent heat release in (1). Thus the dynamical conditions of Figure 3a are artificially imposed on the continental and maritime clouds. Figure 11 displays the vertical cross sections of the SO_2 mixing ratio for both clouds. The continental cloud is more efficient than the maritime one for SO_2 scavenging. Clearly, a rapid SO_2 disappearance occurs as the cloud begins to form in the zone where condensation processes act upwind of the mountain top. The differences observed in the SO_2 fields can be attributed to smaller continental droplets with longer residence times than maritime cloud ones [Hong and Carmichael, 1983; Chameides, 1984].

3.5. Sulfate Deposition

Deposition is the ultimate stage in a chain of very complex interactions between pollutants, winds, clouds, and rain. It

represents a concrete and measurable parameter useful in comparative studies. In Figure 12, comparative tests are synthesized in the form of wet sulfate deposition (in micrometers) accumulated over a 6-hour period. The amount of deposited sulfate is larger in the maritime case (Figure 12b) than in the continental one (Figure 12a). The shift in the maxima of sulfate deposition between the two cases is probably associated with the precipitation drift already discussed in section 2.2). Another test which has been performed bears upon the sensitivity of sulfate deposition to SO_2 oxidation in aqueous phase. The foremost observation in Figure 12, by comparing dashed lines with solid lines, is that the SO_2 scavenging only accounts for a small fraction of the overall pollutant deposition in the continental case. It looks more important in the maritime case, for which it is about one third of the overall sulfate deposition in the first 2 hours of the simulation (Figure 12b).

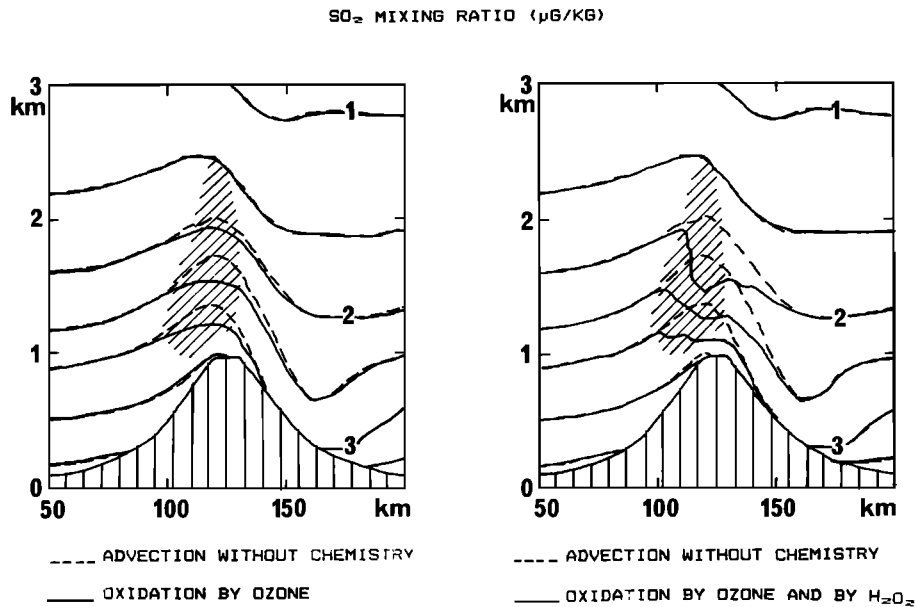


Fig. 9. Vertical cross sections of the SO₂ mixing ratio in maritime clouds after 0.5 hour: (a) without chemistry (dashed line) and with oxidation by ozone (solid line), (b) without chemistry (dashed line) and with oxidation by H₂O₂ and ozone (solid line). Shaded zones show the presence of cloud water. The vertical and horizontal scales are indicated.

The differences in Figure 12b are more obvious at the beginning of the simulation because of the oxidation effect of H₂O₂, which acts during the cloud formation.

4. CONCLUSIONS

A quasi-spectral parameterization for liquid water (both cloud water and rainwater) has been included in the framework of a mesoscale model to quantify the interactive processes at work in pollutant wet removal.

First, sensitivity tests have been performed to establish the following hierarchy among physicochemical processes. Nucleation scavenging has been found to be the most efficient in-cloud scavenging process. Its computation requires knowledge of an explicit nucleation rate and is a function of supersaturation and cloud spectrum. During the cloud formation a

part of total wet deposition is due to SO₂ scavenging, which itself is dependent upon the liquid water content and the droplet sizes. It should be emphasized that the spectral information given by our microphysical scheme is well suited to the treatment of SO₂ dissolution and oxidation in liquid phase, due to detailed representation of the condensation/evaporation processes. In addition, Brownian and turbulent diffusions may significantly contribute to in-cloud scavenging, in the case of small continental droplets capturing particles with radii less than 0.1 μm. Through its quasi-spectral treatment of both hydrometeors and aerosols, the model has the ability to duplicate such effects.

The second point to be emphasized is the methodology adopted for studying typical continental and maritime clouds through idealized tests. In the mesoscale, simultaneous col-

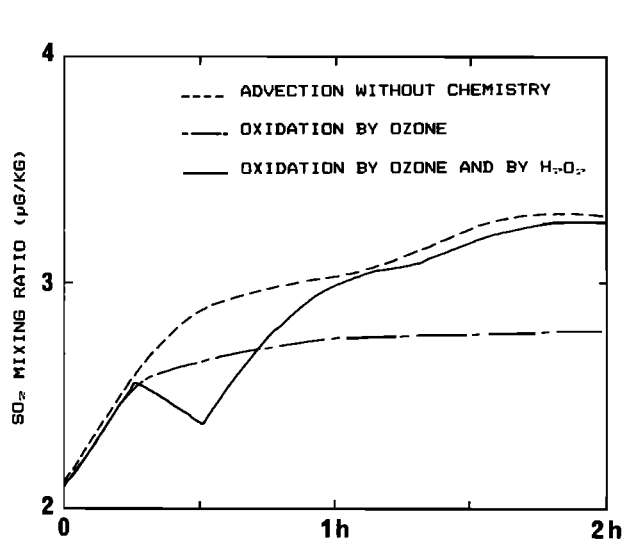


Fig. 10. Temporal evolution of SO₂ mixing ratio over 2-hour period at $x = 110$ km and $z = 150$ m for three sensitivity tests: (a) without chemistry, (b) with oxidation by ozone, and (c) with oxidation by ozone and H₂O₂.

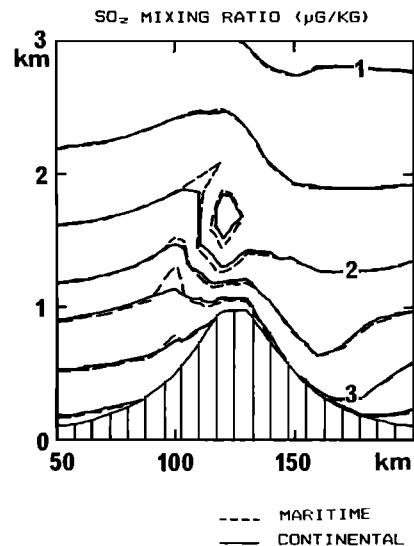


Fig. 11. Vertical cross sections of SO₂ mixing ratio for maritime (dashed lines) and continental (solid lines) clouds after 0.5 hour, with oxidation by H₂O₂ and ozone. Latent heat release effects have been removed.

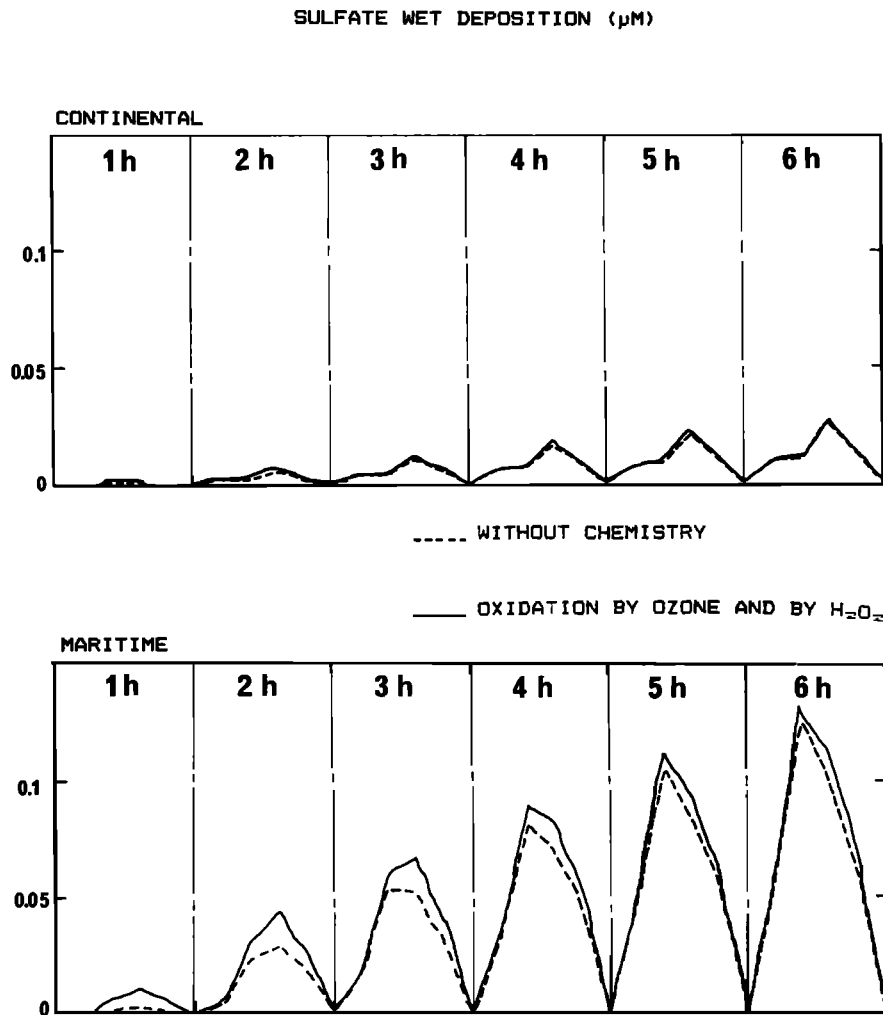


Fig. 12. Temporal evolution of sulfate wet deposition on the mountain top over 6-hour period for continental versus maritime cases for two sensitivity runs: (a) without chemistry (dashed lines) and (b) with oxidation by ozone and H_2O_2 (solid lines).

lection of meteorological and physicochemical data is difficult to carry out experimentally. The results of this study suggest that a comprehensive numerical model could be effective in isolating the underlying interactions of winds, microphysics, and physicochemistry and should be able to discriminate between their relative effects. This can be of use in defining experimental strategies or in interpreting data. Sulfate deposition is very sensitive to the cloud type: in-cloud scavenging is favored in continental clouds, while precipitating maritime clouds remove particles more efficiently. Here only very simple chemistry has been incorporated in the mesoscale model. In particular, a ionic balance equation should be included in the model in order to have more consistency between the pH and the sulfate particle population. Also, because of its explicit representation of the cloud droplet size distribution, the effect of mass transport limitations on SO_2 aqueous-phase oxidation will be studied in the future.

APPENDIX: LIST OF SYMBOLS

C empirical constant (3500 cm^{-3} in continental case, 100 in maritime case).
 C_{ap} dry aerosol concentration.
 $C_{ap\text{-}nuc}$ number of aerosols activated through nucleation during one time step.

C_{cp} cloud water aerosol concentration.
 C_p specific heat at constant pressure for dry air.
 C_{pm} specific heat at constant pressure for moist air.
 C_{rp} removed aerosol concentration.
 D_c cloud droplet diameter.
 D_{c0} distribution parameter for the lognormal cloud droplet distribution.
 D_{crit} minimum critical diameter of (soluble) particles activated at supersaturation S_{max} .
 D_r raindrop diameter.
 D_{r0} distribution parameter for the lognormal raindrop distribution.
 D_v water vapor diffusivity.
 F_X friction terms relative to any prognostic variable X .
 K thermal conductivity.
 K_H horizontal diffusion coefficient.
 L_v vapor latent heat.
 N cloud condensation nucleus concentration.
 N_{cw} cloud droplet concentration.
 N_{nuc} number of cloud droplets nucleated during one time step.
 N_{rw} raindrop concentration.
 P Pressure.
 P_0 reference pressure (1013 mbar).

P_s pressure at the lower boundary.
 P_T pressure at the top boundary.
 $\bar{P} = (P/P_0)^{\kappa}$.
 R specific gas constant for dry air.
 Re Reynolds number.
 R_w specific gas constant for moist air.
 S supersaturation.
 Sc Schmidt number.
 S_n sedimentation flux of raindrops.
 S_{max} maximal supersaturation.
 T temperature.
 $X = Re^{1/2} Sc^{1/3}$.
 e_{sw} saturation vapor pressure over plane water surface.
 \bar{f} ventilation factor.
 g acceleration of gravity.
 i Van't Hoff coefficient for nonideal aqueous salt solution (= 3).
 k empirical constant (0.9 in continental case, 0.7 in maritime case).
 m nucleus mass.
 m_N molecular weight of salt ($= 132.1 \times 10^{-3}$ for $(NH_4)_2SO_4$).
 m_w molecular weight of water.
 q_{ap} dry aerosol volume mixing ratio.
 $q_{ap,nuc}$ volume mixing ratio of aerosols activated through nucleation during one time step.
 q_{cp} cloud water aerosol volume mixing ratio.
 q_{cw} cloud water mixing ratio.
 q_{ds} SO_2 mixing ratio.
 q_{nuc} mixing ratio for cloud droplets nucleated during one time step.
 q_{rp} removed aerosol volume mixing ratio.
 q_{rw} rainwater mixing ratio.
 q_v vapor mixing ratio.
 q_{vs} saturation vapor mixing ratio.
 r_{nuc} nucleus radius.
 t time.
 x horizontal west-east coordinate.
 y horizontal south-north coordinate.
 z altitude.
 β beta function;
 $\beta(a, b) = \int_0^1 x^{a-1} (1-x)^{b-1} dx$.
 ε constant (= 0.623).
 ρ_a density of air.
 ρ_w density of water.
 v vertical coordinate defined by $\sigma = (4v - v^4)/3$.
 \dot{v} vertical velocity.
 π constant (= 3.141592653).
 Π ground pressure ($= P_s - P_T$).
 κ constant (= 2/7).
 σ pressure coordinate defined by $\sigma = (P - P_T)/\Pi$.
 σ' $d\sigma/dv$.
 σ_c dispersion parameter for lognormal cloud droplet distribution (0.15 for continental cloud and 0.28 for maritime cloud).
 σ_r dispersion parameter for lognormal raindrop distribution (= 0.5).
 Θ potential temperature.

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