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Are eruptions from linear fissures and caldera ring dikes more likely to produce pyroclastic flows?

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Abstract

Turbulent volcanic jets are produced by highly-energetic explosive eruptions and may form buoyant plumes that rise many tens of kilometres into the atmosphere to form umbrella clouds or collapse to generate ground-hugging pyroclastic flows. Key to which of these two behaviours will occur is the extent to which the mechanical entrainment and mixing of ambient air into the jet by large (entraining) eddies forming the jet edge changes the density of the air-ash mixture: low entrainment rates lead to pyroclastic flows and high entrainment rates give rise to buoyant plumes. Recent experiments on particle-laden (multi-phase) volcanic jets from flared and straight-sided circular openings suggest that the likelihood for buoyant plumes will depend strongly on the shape and internal geometry of the vent region. This newly recognised sensitivity of the fate of volcanic jets to the structure of the vent is a consequence of a complex dynamic coupling between the jet and entrained solid particles. Building on this work, here we use an extensive series of experiments on multi-phase turbulent jets from analogue linear fissures and annular ring fractures to explore whether the restrictive vent geometry during cataclysmic caldera-forming (CCF) eruptions will ultimately lead a relatively greater frequency of pyroclastic flows than eruptions from circular vents on stratovolcanoes. Our results, understood through scaling analyses and a one-dimensional theoretical model, show that entrainment is enhanced where particle motions contribute angular momentum to entraining eddies. However, because the size of the entraining eddies scales approximately with vent width, the extent of entrainment is reduced as the vent width becomes small in comparison to its length. Consequently, our work shows that for specified mass eruption rates, the high length-to-width ratio vents typical of CCF events are more likely to produce pyroclastic flows. We suggest that the enigmatic proclivity in the geological record for the largest CCF eruptions to produce pyroclastic flows is an expected consequence of their being

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erupted through continuous or piece-wise continuous caldera ring fractures.

Keywords:

Turbulent Entrainment; Volcanic Jets; Pyroclastic Flows; Caldera Formation; Column Collapse

1. Introduction

Volcanic jets are turbulent, particle-laden (multi-phase) flows that may rise as a buoyant plume high into the atmosphere, forming an umbrella cloud, or undergo catastrophic gravitational collapse to produce devastating pyroclastic flows (PFs). Which of these behaviours occurs depends on the source conditions governing the strength and shape of the jet (e.g. Wilson et al., 1980, and references therein), the stratification (i.e. density profile) of the atmosphere and, more critically, on the extent to which ambient air is entrained into the jet (e.g. Woods, 2010). A remarkable feature in the deposits related to the largest catastrophic caldera-forming (CCF) events is that ignimbrites formed by pyroclastic flows are commonly much more voluminous than deposits resulting from ash fall out from sustained buoyant plumes (e.g. Lipman, 1984; Cole et al., 2005; Cas et al., 2011; Ferguson et al., 2013). Furthermore, many caldera-related deposit sequences consist of basal ash-fall layers with upper thick ignimbrites, suggesting a shift in eruptive dynamics (Druitt and Sparks, 1984).

The size of eruptions can be inferred from the volume of their deposits using the magnitude scale (Mason et al., 2004),

$$M = \log_{10}(\rho_b V_t) - 7 \quad (1)$$

where ρ_b is the bulk density and V_t is the total erupted (bulk) volume. For a volume of ignimbrite, V_i , the ratio V_i/V_t generally correlates with M but, as figure 1 shows, the slope suddenly increases beyond a certain “critical” magnitude which we take to be $M_{\text{crit}} \approx 7.5$ and which corresponds roughly to the transition from the “hyperactive” to “super-eruption” regime (Jellinek and DePaolo, 2003; Jellinek, 2014). In the latter, magma is stored gradually over time, rather than being erupted periodically, in very large magma chambers that form large calderas and large deposits when they eventually erupt (Mason et al., 2004). Whether this correlation is a significant indicator of the distinctive dynamics of such caldera-forming eruptions compared to eruptions from circular vents on stratovolcanoes, or simply a consequence of preservational bias is unclear. Super eruptions have $M > 8$ (i.e. $V_t > 400 \text{ km}^3$) and occur infrequently, roughly every 10^4 – 10^5 years on the global scale, and eject 10^3 – 10^4 km^3 of pyroclastic material (Smith, 1960; Mason et al., 2004; Wilson, 2008; Miller and Wark, 2008). A provocative issue is, thus, whether caldera eruption columns are unstable simply because of their large size or whether

28 their typical eruption column dynamics are being influenced by the linear or annular vents through
 29 which material is injected into the atmosphere.

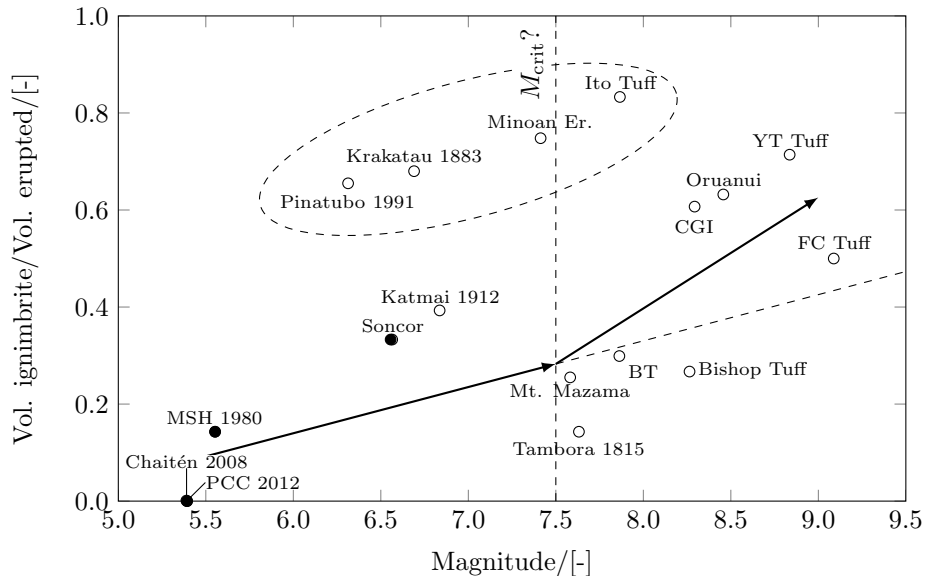


Figure 1: Ratio of ignimbrite volume, V_i , to total magma volume, V_t , produced for 17 historic and pre-historic silicic eruptions as a function of the eruption magnitude, $M = \log_{10}(\text{erupted mass}/[\text{kg}]) - 7$. The arrows give a suggested trend for the ignimbrite/total volume ratio with magnitude. Details of the eruptions are given in §5.3. The caldera-forming eruptions shown are, in order of decreasing magnitude: Fish Canyon Tuff (FC Tuff); Younger Toba Tuff (YT Tuff); Oruanui Ignimbrite; Cerro Galán Ignimbrite (CGI); Bishop Tuff; Ito Tuff; Bandelier Tuff (BT); Tambora 1815; Mount Mazama; Santorini (Minoan eruption); Katmai 1912; Krakatau 1883; Pinatubo 1991; Chaitén 2008. Three non caldera-forming eruptions are shown for reference with filled points: Lascar (Soncor); Mt. St. Helens 1980/05/18 (MSH 1980); Puyhue-Cordón Caulle 2012 (PCC 2012). References for these deposits/eruptions can be found in the supplementary material.

30 Typically, the rate of turbulent entrainment is characterised by relating the inflow rate of ambient
 31 air to the mean rise rate of a turbulent jet through an entrainment coefficient (Morton et al., 1956),

$$32 \quad \alpha_e \equiv u_{\text{in}}/\bar{u}, \quad (2)$$

33 where u_{in} is the speed at which ambient air is entrained into the jet and \bar{u} is the mean vertical jet
 34 velocity (Morton et al., 1956; Woods, 2010, and figure 2). It is commonly assumed that α_e is a constant
 35 with values in the range 0.1 for momentum dominated jets to 0.15 for buoyant plumes (Morton et al.,
 36 1956; Fischer et al., 1979), though more recent work has shown that α_e may in fact vary as the
 37 buoyancy, velocity and turbulent shear stress profiles evolve with height (Kaminski et al., 2005; Paillat
 38 and Kaminski, 2014a).

39 A mechanical clue to the potential for differing dynamics of entrainment into volcanic jets from
 40 circular, linear and annular vents is illustrated in figure 2. We infer from experimental investigations

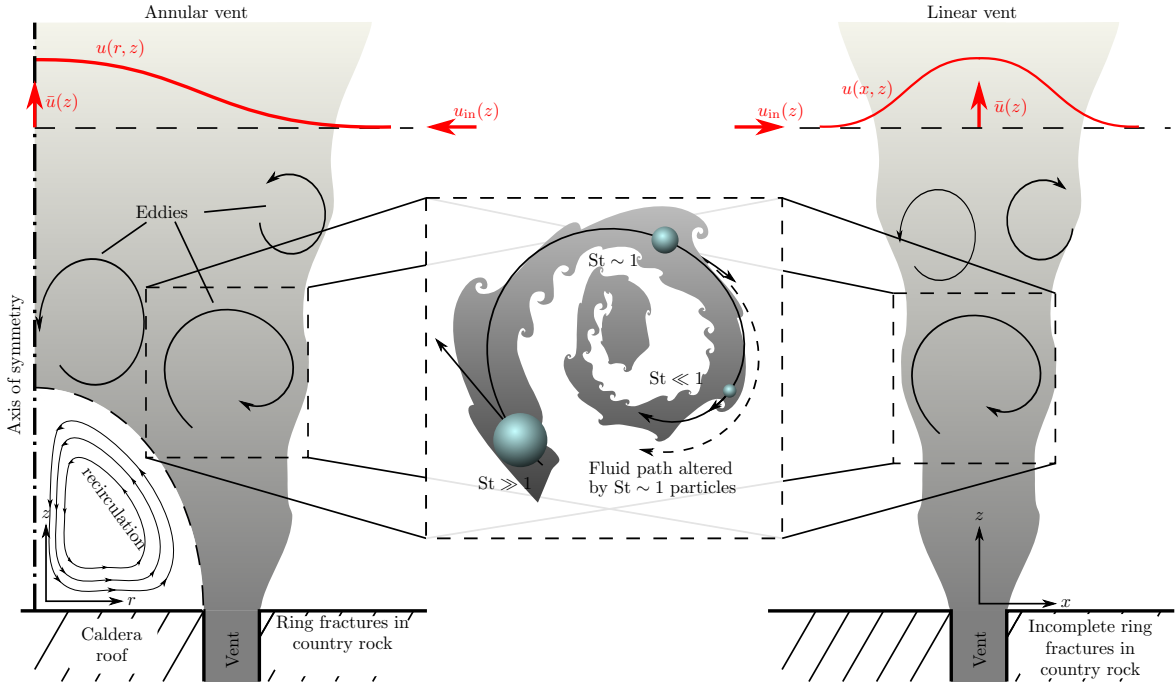


Figure 2: Schematics of the turbulent structure of a volcanic jet from (left) an annular vent and (right) from a linear vent. We show the time-averaged velocity profiles, $u(r, z)$ and $u(x, z)$ (—) and a region of recirculation just above the annular vent. (Inset) particle-eddy coupling regimes according to St . Particles with $St \sim 1$ can stretch the eddies to which they are coupled.

41 of incompressible jets from annular vents that, just downstream of the caldera roof, a zone of steady
 42 recirculation forms and that the jet remains annular for some distance (e.g. Ko and Chan, 1978;
 43 Del Taglia et al., 2004). This annular flow causes the dynamics of the jets with annular vents to differ
 44 from jets with circular vents, notably in the strain rates ($\dot{\gamma} \approx \bar{u}/l$) close to the vent which, in turn,
 45 affect entrainment into the jet.

46 Vent geometry affects the dynamics of a multi-phase volcanic jet in two ways: i) the cross-sectional
 47 area modulates the mass eruption rate (MER), and eruptions with high MER tend to produce jets
 48 that rise high into the atmosphere to form buoyant plumes, whereas low MER eruptions tend to form
 49 collapsing fountains (Wilson, 1976); ii) vent shape and internal geometry influences the structure of
 50 entraining eddies as well as the trajectories of inertial particles with knock-on effects for the ability of
 51 the relatively dense jet to entrain ambient air and become buoyant (Jessop and Jellinek, 2014). The
 52 effect of vent geometry has been explored in the context of particle-free, trans-sonic volcanic jets (e.g.
 53 Wilson et al., 1980; Koyaguchi et al., 2010; Ogden, 2011). Under these conditions, vent radius, crater
 54 structure and pressure at the vent govern the MER.

55 Entrainment into jets from linear vents without particles has been well studied (e.g. Kotsovinos,

56 1977; Paillat and Kaminski, 2014b). In experiments on jets from vents that are much longer than they
 57 are wide, velocity profiles across the widths of these flows are similar in form to those characteristic
 58 of axisymmetric jets (Morton et al., 1956). Consequently, a similar entrainment hypothesis (cf eq. 2)
 59 can be applied along with similar conditions for the likelihood that a volcanic jet will rise as a buoyant
 60 plume or collapse to form a pyroclastic flows.

61 Because of the high vent aspect ratio of jets erupted from fissures Glaze et al. (2011) proposed that
 62 such eruptions will inevitably involve more extensive entrainment relative to jets from circular sources
 63 for specified mass eruption rates. Whether this picture is true and how it is affected by the particulate
 64 component of eruptions is unclear. More generally though, most previous works assume implicitly that
 65 the major effect of particles is to contribute only to the bulk density of the flow (Veitch and Woods,
 66 2000). Models for jet evolution based on the entrainment hypotheses consequently require either that
 67 particles are perfectly coupled (i.e. the particles exactly follow fluid streamlines) and contribute to the
 68 mean physical properties of the flow or else that the particles decouple from the flow and sediment
 69 quasi-instantaneously from the jet margins and play no further role in driving flow of the jet (e.g.
 70 Woods, 1988). A useful metric for particle-fluid stress coupling in a turbulent flow is the Stokes
 71 number,

$$72 \quad \text{St} = \frac{\tau_p}{\tau_e} = \frac{\rho_p d_p^2 u_e}{18 f \mu l_e}, \quad (3)$$

73 which is a ratio of the response time of a particle τ_p to flow accelerations imparted on an eddy overturn
 74 time $\tau_e \sim l_e/u_e$, where u_e is proportional to the mean vertical flow speed. In (3), ρ_p and d_p are the
 75 particle density and diameter, respectively, μ is the fluid dynamic viscosity, f is a drag factor of $\mathcal{O}(1)$
 76 (Burgisser et al., 2005). Three different particle-fluid coupling regimes can be defined according the
 77 value of St:

$$78 \quad \text{St} = \begin{cases} \ll 1 & \text{Stokesian - one-way (fluid-particle) coupling} \\ \sim 1 & \text{Inertial - two-way "critical" coupling} \\ \gg 1 & \text{Ballistic - one-way (particle-fluid) coupling} \end{cases}$$

79 Particle motions are affected by flow accelerations and the structures and momentum fluxes carried
 80 by eddies within the flow are, in turn, altered by particle accelerations when $\text{St} \sim 1$ (figure 2, inset,
 81 Burgisser et al., 2005, and references therein). In this two-way coupling regime, particles are “critically
 82 coupled” to the flow, and we will refer to them as “inertial particles”. By contrast, particles with $\text{St} \ll 1$

83 are assumed to be perfectly coupled to eddies and particles with $St \gg 1$ are decoupled from the flow
84 entirely and follow ballistic trajectories. Whereas perfect coupling or sedimentation may be true of
85 the very smallest or largest particles, respectively, volcanic jets contain pumices, ash and lithic clasts
86 of a very wide range of grain sizes, a certain portion of which are critically coupled to the flow and
87 may hence influence the entraining properties of the jet (Crowe et al., 1997; Raju and Meiburg, 1997;
88 Burgisser et al., 2005). To put these regimes into the volcanological context, we have calculated St
89 based on the grain size distribution (GSD) and source/jet conditions in two well-studied eruptions:
90 1979 Soufrière, St. Vincent (SSV), and 1980 Mount St. Helens (MSH), USA. We note that MSH was
91 about 100 times greater in eruption magnitude than SSV. Details of our calculations are given in the
92 supplementary material. We find that 32% of the GSD has $St = \mathcal{O}(1)$ for the SSV eruption and 18%
93 for the MSH eruption. Here we infer by $St = \mathcal{O}(1)$ the portion of the distribution with $0.3 \leq St \leq 3$.
94 These calculations show that particles with $St = \mathcal{O}(1)$ represent a significant volumetric fraction of
95 jets generated in explosive volcanic eruptions. In addition to the effects of particle-fluid coupling on
96 entrainment, particle sedimentation from the jet margins can also affect the mean density and internal
97 dynamics of these flows. Particle sedimentation from the jet margins can be quantified through a
98 settling number, $\Sigma_s = v_s(d_p)/\bar{u}$ where $v_s(d_p)$ is the settling velocity of particles of size d_p (Burgisser
99 et al., 2005). Under most natural conditions, however, settling of $St \sim 1$ particles is a much slower
100 process compared to eddy overturning in the jet and the inertial timescales of these particles. Hence
101 sedimentation has a negligible effect on the dynamics of the jet (Woods and Bursik, 1991; Carazzo and
102 Jellinek, 2012; Jessop and Jellinek, 2014).

103 In most studies, the explicit and coupled mechanical effects of the three-dimensional geometry of a
104 vent and the presence of inertial particles in the jet on entrainment are neglected. Jessop and Jellinek
105 (2014), henceforth referred to as JJ14, showed that $St \sim 1$ particles influence entrainment because vent
106 geometry influences the trajectories of inertial particles and these, in turn, stretch the entraining eddies
107 (see inset of Fig. 2). In particular, particles ejected from flared vents contribute angular momentum
108 to and increase the size of entraining eddies, hence enhancing entrainment. Particles ejected from
109 straight-sided vents carry momentum vertically to produce thin, stretched eddies to hence reduce
110 entrainment. As the combination of vent shape and inertial particles affects the mixing of the jet,
111 the structure of the ash cloud and hence the sedimentation regime are affected in turn (Carazzo and
112 Jellinek, 2012). This result predicts substantially different ash-fall deposit architectures produced by
113 jets from straight-sided and flared vents and an evolution in sedimentation regime with vent erosion

114 during an eruption (Carazzo and Jellinek, 2012, JJ14). This picture is in marked contrast to previously
115 proposed models for the dynamics of volcanic jets that generally assume a point source (e.g. Woods,
116 1988, 2010).

117 Although the straight and flared circular vent geometries discussed in JJ14 are typical of eruptions
118 from stratovolcanoes, eruptions from linear fissures and ring dikes related to caldera subsidence, which
119 may in part be structurally controlled, dominate the geological record of caldera-forming eruptions (e.g.
120 Lipman, 1997; Aguirre-Diaz and Labarthe-Hernandez, 2003; Mason et al., 2004; Kennedy et al., 2008;
121 Cole et al., 2010). During caldera-forming events, subsidence of relatively thin, laterally-extensive
122 chamber roofs and along continuous (e.g. Mt. Mazama, Bacon, 1983; Long Valley Caldera, Hildreth
123 and Mahood, 1986; Wilson and Hildreth, 1997) or partly continuous (e.g. Poris formation, Brown and
124 Branney, 2004; Permian Ora Ignimbrite, Willcock et al., 2013; Bad Step Tuff, Branney et al., 1992)
125 ring fractures probably follows initial chamber decompression (Druitt and Sparks, 1984; Roche and
126 Druitt, 2001) and ultimately drives a protracted eruption through a ring dike with geometric properties
127 that vary as the eruption proceeds (e.g. Druitt and Sparks, 1984; Lipman, 1984; Hildreth and Mahood,
128 1986; Folch and Martí, 2004; Kennedy et al., 2008).

129 Large-volume and large MER eruptions from purely linear vents (e.g. a dyke extending to the
130 surface) have been inferred purely from field data (e.g. Soldier Meadow Tuff, Korringa, 1973) and from
131 field data along with contemporary observations (Tarawera 1886, Walker et al., 1984) and yet it has
132 not been well understood how a linear vent could retain its shape and hence sustain a high MER,
133 and not evolve to a more stable, circular form with a more restricted MER. Recently, however, Costa
134 et al. (2011) showed that in regions of crustal extension (e.g. Taupo, NZ; Sierra Madre Occidental,
135 Mexico Aguirre-Diaz and Labarthe-Hernandez, 2003; Cole et al., 2010, for example), even moderate
136 extensional stress (40 MPa) is sufficient to sustain the linear vent shape and thus produce very large
137 MER ($\sim 10^{10}$ kg/s) eruptions.

138 In this paper, we use experiments, theory and field data analysis to test and confirm the hypothesis
139 that the particular mechanics of entrainment into multi-phase volcanic jets erupting from partial (piece-
140 wise continuous fissures) or complete (continuous) caldera ring dikes ultimately favour jet instability
141 and, in turn, the production of pyroclastic flows. We will argue that CCF events are generally more
142 likely to produce massive ignimbrites than stratovolcanoes and that the remarkably regular occurrence
143 of these deposits with the largest events is expected. Critically, we will show that this expectation is
144 related to not simply the geometry of volcanic vents but also dynamically related to the coupling of

145 these jets to the particles they carry into the atmosphere.

146 2. A simple model for entrainment dynamics

147 In order to entrain and mix ambient fluid (such as atmospheric air) into a turbulent jet, the
 148 eddies at the edge of the jet must do work to penetrate, deform, and overturn the density interface
 149 defining the edge of the jet. The work to ultimately irreversibly mix the jet and ambient fluid is
 150 extracted from the kinetic energy (KE) carried by the jet. The ratio of KE available to the change
 151 in gravitational potential energy in overturning the interface is commonly expressed in terms of a
 152 local Richardson number, $Ri = g'b/\bar{u}^2$ where b and \bar{u} are the local values of jet radius and mean
 153 axial velocity, respectively (e.g. Linden, 1973). The reduced gravity is $g' = g(\rho_a - \rho)/\rho_0$ with ρ , ρ_a
 154 and ρ_0 the densities of the jet, local ambient fluid and a reference location (typically taken to be the
 155 density of the ambient fluid at the level of the vent), respectively, and g the gravitational acceleration.
 156 Ri equally expresses the local balance between stabilising buoyancy and destabilising inertial forces
 157 (Linden, 1973). However, as a metric for jet strength in our experiments, it is convenient to define Ri
 158 in terms of conditions controlled at the source,

$$159 \quad Ri_0 = \frac{g'_0 L_0}{\bar{u}_0^2}, \quad (4)$$

160 where, for all variables, a subscript 0 represents a value at the source, $L_0 = \sqrt{A_0/\pi^s}$ is a length scale
 161 for a given nozzle shape defined by the flux through the opening area, A_0 and $s = 0$ for linear vents
 162 and $s = 1$ for annular vents. Rectangular (linear) vents are defined by a width, $2l_w$, and breadth, $2l_b$,
 163 (Fig. 3b) hence $A_0 = 4l_b^2/\epsilon$ where $L_0 = 2l_b\epsilon^{-1/2}$ and $\epsilon = l_b/l_w$. Annular nozzles are defined by a gap
 164 size, d , and overall diameter, d_0 (Fig. 3c) so that $A_0 = \pi d_0^2/4(2\epsilon - \epsilon^2)$ where the nozzle aspect ratio
 165 is $\epsilon = d/d_0$. Therefore, $L_0 = d_0/2\sqrt{2\epsilon - \epsilon^2}$. Ri in the jet evolves with height and, generally, we may
 166 write $Ri \propto |Ri_0|$. A coefficient of proportionality, β , relates $|Ri_0|$ to Ri so we may therefore write, for
 167 an annular vent,

$$168 \quad \beta = \frac{Ri}{|Ri_0|} \propto \left(\frac{\bar{u}_0}{\bar{u}}\right)^2 \frac{1}{\sqrt{2\epsilon - \epsilon^2}}, \quad (5)$$

169 whereas the definition of L_0 for a rectangular nozzle gives

$$170 \quad \beta \propto \left(\frac{\bar{u}_0}{\bar{u}}\right)^2 \sqrt{\epsilon}. \quad (6)$$

171 These two expressions for β indicate the extent to which KE available at the source (i.e. $\text{KE} \sim \bar{u}^2$) is
 172 extracted for mixing, depending on vent geometry, ϵ . However, following JJ14, to simplify discussion
 173 of our results we introduce a more intuitive metric $\lambda = 1/\beta$: when λ is large, more energy is supplied
 174 to do the work of overturning the stratification and cause mixing.

175 Steady jets can be described through coupled equations for the conservation of flux of specific
 176 volume, $q = b^2\bar{u}$, momentum, $m = b^2\bar{u}^2$, and buoyancy, $f = g'b^2\bar{u}$. Equivalently, a closed system
 177 can also be obtained by replacing f by the conservation of particle mass flux, $p = \phi b^2\bar{u}$, and the
 178 effect of dilution on g' (see appendix of Carazzo and Jellinek, 2012). Here, ϕ is the particle volume
 179 fraction (i.e. monodisperse GSD) and thus the jet bulk density is $\rho = (1 - \phi)\rho_a + \phi\rho_s$ where ρ_s is
 180 the particle density. In this case, the effects of environmental stratification are encompassed in the g'
 181 parameter. Particle mass flux is a balance between the upward transport of particles by the jet and
 182 particle loss through sedimentation, though the latter is comparatively small for the jets considered
 183 here. In the “top-hat” formalism (cf. Morton et al., 1956; Woods, 2010) these conservation principles
 184 can be expressed as (for axisymmetric jets)

$$185 \quad \frac{dq}{dz} = 2\alpha_e\sqrt{m}, \quad m\frac{dm}{dz} = g'q^2, \quad \frac{dp}{dz} = 0. \quad (7)$$

186 It is apparent from these relationships that the jet radius can be expressed as $b = q/m^{1/2}$. The jet
 187 angle, θ , is then given by

$$188 \quad \frac{db}{dz} = 2\alpha_e - \frac{|\text{Ri}_0|}{2\lambda} = \tan\theta. \quad (8)$$

189 For a linear jet, an equivalent expression can be obtained by writing the two-dimensional conservation
 190 equations as per Paillat and Kaminski (2014a) and differentiating to obtain

$$191 \quad \frac{db}{dz} = \frac{4}{\sqrt{\pi}}\alpha_e - \frac{\sqrt{2}}{\lambda}|\text{Ri}_0| = \tan\theta. \quad (9)$$

192 The system of equations (7) is sufficient to model the rise and spread of turbulent jets as all the details
 193 of how fluid is entrained into the flow are contained within α_e (Morton et al., 1956). We note that,
 194 for multi-phase flows, α_e must therefore implicitly describe the influence of the source geometry and
 195 inertial particles on entrainment dynamics whereas $\lambda \propto (\bar{u}/\bar{u}_0)^2$ is a measure of how much KE has been
 196 extracted from the flow relative to how much was present at the source. We will make experimental
 197 measurements of θ as a function of the source conditions and use (8) to infer how α_e and λ vary

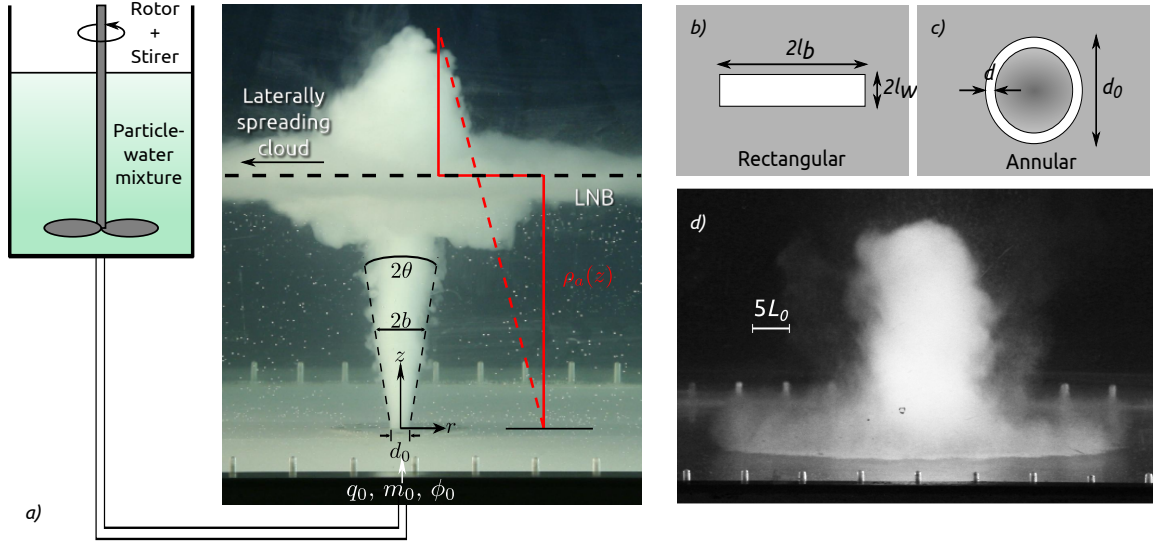


Figure 3: a) Schematic of experimental set up and the measurements taken. Definitions of dimensions for b) rectangular and c) annular vents. An image of a collapsing fountain from an experiment using the linear vent.

198 according to these conditions.

199 3. Experiments

200 We performed isothermal experiments similar to JJ14 where a particle-water mixture was injected
 201 into a tank of water to produce a particle-laden jet (Fig. 3a). The injection rate was constant and
 202 jets were formed through various straight-sided nozzles which had openings that were either annular
 203 or rectangular in cross section (Fig. 3b, c). The resulting turbulent jets had a source Reynolds
 204 number, $Re_0 = \bar{u}_0 D_0 / \nu$, of $\mathcal{O}(10^3)$ or greater (Table 1) indicating fully turbulent conditions in these
 205 unbounded flows. Here, ν is the kinematic mixture viscosity and the length scale D_0 is the narrowest
 206 nozzle gap (d or l_b). We recorded the morphology of these jets and measured the jet opening angle,
 207 2θ , as a function of ϕ_0 , Ri_0 and St_0 as shown in figure 3. We explicitly control these source parameters
 208 so as to reproduce conditions inferred for natural eruptions (Carazzo and Jellinek, 2012, JJ14). In
 209 particular, we note that the values of ϕ_0 are comparable to natural eruptions as discussed in Appendix
 210 A.1 (supplementary material). In some experiments, a density stratification was achieved by adding
 211 a lower layer of salty water and carefully filling the rest of the tank with fresh water. This “two-
 212 layer” setup has been shown to reproduce the effects of more realistic quasi-linear density gradients if
 213 the density difference and layer height are carefully chosen to match the value of the linear gradient

214 (Carazzo and Jellinek, 2012). Although injected mixtures are always denser than the ambient fluid at
215 the source, entrainment, dilution and particle loss can cause the jets to become buoyant plumes (e.g.
216 Woods, 2010; Carazzo and Jellinek, 2012). Some of our experiments consequently produce buoyant
217 plumes while others lead to collapsing fountains. In other experiments, only fresh water was used to
218 fill the tank (Table 1).

219 We used particles with a mean diameter of $250 \mu\text{m}$ and standard deviation of $50 \mu\text{m}$, determined
220 by passing the materials through a graded range of sieves. All the particles were made of silica and had
221 a density of 2.5 g/cm^3 . The particles were chosen so that, for the largest eddies formed at the source,
222 $\text{St}_0 = \mathcal{O}(0.1 - 1)$. The particle size and typical experimental conditions give $\Sigma_{s0} = \mathcal{O}(0.01 - 0.1)$
223 (Table 1).

224 We measured the angle from the vertical of the jet, θ , from a stack of 3–5 images taken from a digital
225 camera each taken at intervals of $\sim 1 \text{ s}$ and infer the steady-state entrainment from this information
226 via (8). We carefully manufactured our annular vents to ensure that they were as symmetric as
227 possible so no variation in entrainment rate linked to varying gap size around the vent was observed
228 in the experiments. Finally, we noted whether the jet formed in each experiment formed a buoyant
229 plume or a collapsing fountain and these findings are reported in Table 1. Because buoyancy reversals
230 cannot occur in unstratified environments, we only report collapsing fountains for experiments with
231 stratification.

232 4. Results

233 We present our results for θ as a function of Ri_0 in figure 4. Figure 4a shows results for the annular
234 nozzles of different ϵ , whereas Fig. 4b shows the same parameter space for a rectangular nozzle with
235 $\epsilon = 0.41$. We show solutions to (8) fitted to the data of JJ14 for narrow and broad/flared vents for
236 particle-free and particle-laden jets. Also, to aid interpretation, we have included “isoentrainment”
237 curves which are solutions to (8) with constant α_e and λ : the vertical differences in the isoentrainment
238 curves represent the different values of α_e (curves are higher for larger α_e) whereas horizontal differences
239 represent different values of λ , so that the “roll-off” is quicker for smaller λ . The source particle
240 concentration, ϕ_0 is indicated by a colour scale.

241 In general, θ increases with ϵ of annular nozzles. In addition particle-laden jets correspond to
242 larger values of α_e and higher values of λ . Particle-free jets from the $\epsilon = 0.42$ annular vent correspond
243 approximately to iso-entrainment curves with $\alpha_e \approx 0.125$ and $\lambda \approx 1$ (Fig. 4a). Approximately particle-

Table 1: Experimental conditions used in this study. A dash in the St_0 and Σ_{s0} fields indicates that no particles were present for that experiment. When the tank was stratified, we report whether the experiment formed a buoyant plume (BP) or a collapsing fountain (CF).

Expt.	Nozzle Shape	ϵ	ϕ_0	Re_0	St_0	Σ_s	$-Ri_0$	Class
1	annular	0.09	0.000	10 347	–	–	3.46×10^{-7}	–
2	annular	0.09	0.000	14 225	–	–	8.42×10^{-6}	–
3	annular	0.09	0.000	13 929	–	–	3.50×10^{-4}	–
4	annular	0.09	0.009	18 182	0.92	0.02	4.20×10^{-4}	–
5	annular	0.09	0.009	13 475	0.67	0.03	1.08×10^{-3}	–
6	annular	0.09	0.009	14 014	0.59	0.03	9.19×10^{-3}	–
7	annular	0.09	0.019	12 958	0.56	0.03	1.11×10^{-2}	–
8	annular	0.26	0.000	9 896	–	–	1.16×10^{-5}	–
9	annular	0.26	0.000	9 912	–	–	1.02×10^{-4}	–
10	annular	0.26	0.003	4 378	0.28	0.06	1.27×10^{-5}	BP
11	annular	0.26	0.009	4 409	0.29	0.06	3.34×10^{-4}	BP
12	annular	0.26	0.019	3 832	0.26	0.07	7.10×10^{-4}	CF
13	annular	0.26	0.019	3 268	0.22	0.08	1.59×10^{-2}	CF
14	annular	0.42	0.000	3 387	–	–	6.49×10^{-5}	BP
15	annular	0.42	0.000	6 422	–	–	3.66×10^{-4}	–
16	annular	0.42	0.000	3 617	–	–	2.64×10^{-2}	CF
17	annular	0.42	0.000	3 398	–	–	3.28×10^{-2}	CF
18	annular	0.42	0.009	7 768	0.09	0.12	2.24×10^{-2}	–
19	annular	0.42	0.020	6 260	0.07	0.14	5.40×10^{-3}	–
20	annular	0.42	0.020	7 061	0.08	0.13	5.73×10^{-3}	CF
21	annular	0.42	0.000	4 345	–	–	6.03×10^{-3}	BP
22	linear	0.41	0.000	6 495	–	–	9.53×10^{-5}	–
23	linear	0.41	0.000	6 571	–	–	1.89×10^{-2}	–
24	linear	0.41	0.005	6 373	0.28	0.04	3.23×10^{-5}	BP
25	linear	0.41	0.009	6 524	0.29	0.04	7.77×10^{-4}	BP
26	linear	0.41	0.019	18 435	1.48	0.01	2.33×10^{-4}	CF
27	linear	0.41	0.019	15 970	1.26	0.02	5.80×10^{-4}	CF
28	linear	0.41	0.019	5 061	0.23	0.05	8.56×10^{-3}	CF
29	linear	0.41	0.022	5 800	0.26	0.04	8.16×10^{-5}	BP
30	linear	0.41	0.032	6 002	0.28	0.04	3.53×10^{-5}	BP

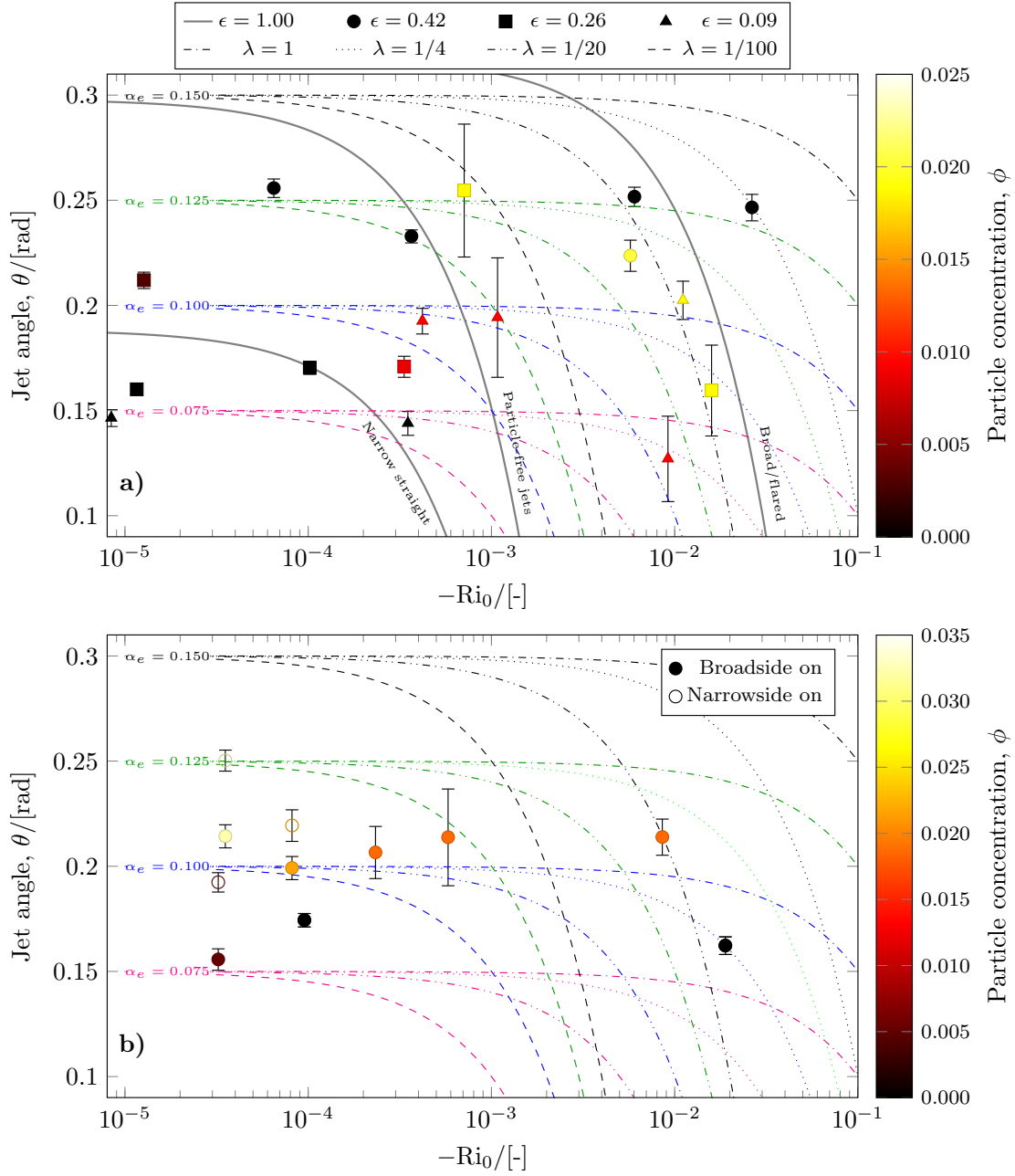


Figure 4: Measured jet angles as a function of $-Ri_0$ for (a) annular nozzles and (b) a linear nozzle ($\epsilon = 0.41$), where filled and empty symbols represent measurements taken along the broad and narrow sides of the jet. The different shaped symbols in (top) represent different values of ϵ . The colour of the symbol represents the particle concentration, ϕ . We show solutions to (8) (isoentrainment curves) fitted to the data from JJ14 in a) ($\epsilon = 1$) for narrow (straight-sided) nozzles, broad and/or flared nozzles and particle-free jets. We also show solutions to (8) as dotted/dashed curves to aid interpretation of the new data.

Table 2: Values of α_e and λ for the different vent and particle concentrations tested.

Nozzle	ϵ	Condition/ ϕ	α_e	λ
8/9	0.42	Particle free/ $\phi \approx 0$	0.125	0.25
8/9	0.42	Particle laden	–	–
10	0.26	Particle free/ $\phi \lesssim 0.01$	0.100	0.01
10	0.26	Particle laden/ $\phi = 0.019$	0.125	0.05
12	0.09	Particle free	0.075	0.01
12	0.09	Particle laden	0.100	0.05
11	0.41	$\phi \lesssim 0.005$	0.075	1
11	0.41	$\phi = 0.019$	0.100	1
11	0.41	$\phi = 0.032$	0.125	1

244 free jets from the vent with $\epsilon = 0.26$ correspond to $\alpha_e \approx 0.075$, $\lambda \approx 0.01$ whereas higher concentration
 245 jets from a vent with the same ϵ have $\alpha_e \approx 0.125$, $\lambda \approx 0.05$. The jet angles formed by jets with $\phi \approx 0$
 246 from the vent with $\epsilon = 0.09$ suggest that $\alpha_e \approx 0.075$ and $\lambda \approx 0.01$ whereas more concentrated jets
 247 have $\alpha_e \approx 0.1$ and $\lambda \approx 0.05$. We summarise these results in table 2.

248 For rectangular vents, a distinctive feature is that the jet angles parallel and perpendicular to the
 249 long axes of the vent are not equal (figures 4b, 5a, b), and λ that is almost 5 times larger. Furthermore,
 250 we find that θ is systematically smaller parallel to the long axis of the jet than perpendicular to the
 251 long axis. However, over a vertical distance of about 10–15 L_0 the jet width evolves to be approximately
 252 equal in both directions, as indicated in figures 5a, b where the widths at 15 L_0 cm are identical. This
 253 suggests that the jets from a linear vent with $\epsilon = 0.41$ eventually become axisymmetric, which is
 254 further evidenced by the approximately circular deposits (Fig. 5c). We acknowledge, however, that
 255 smaller ϵ may produce only elliptical deposits. Particle-laden jets from this linear nozzle ($\phi \approx 0.02$)
 256 had $\alpha_e \approx 0.1$ and $\lambda \approx 1$. For nearly equivalent Ri_0 , larger ϕ increased θ , indicating a larger α_e , whereas
 257 jets with $\phi \approx 0$ had a decreased θ , indicating lower α_e .

258 Using our estimations for α_e and λ for the different vent shapes, ϵ and ϕ (resumed in table 2) we
 259 derived the proportion of source to local KE, noting that $(\bar{u}/\bar{u}_0)^2 \propto \lambda f(\epsilon)$ with $f(\epsilon)$ given by (5) and
 260 (6). The effect of ϵ on $(\bar{u}/\bar{u}_0)^2$ is shown in figure 6. We find that, for $\phi = 0$ from an annular vent,
 261 $(\bar{u}/\bar{u}_0)^2$ decreases with decreasing ϵ . For an annular vent with $\phi > 0$, $(\bar{u}/\bar{u}_0)^2$ increases by nearly an
 262 order of magnitude as ϵ increases from 0.09 to 0.26. Whereas we do not have enough data to establish
 263 trends for $\phi > 0$ in rectangular vents of any ϵ , for an approximately equivalent ϵ and $\phi = 0$, $(\bar{u}/\bar{u}_0)^2$
 264 is about an order of magnitude greater for a linear vent than an annular vent.

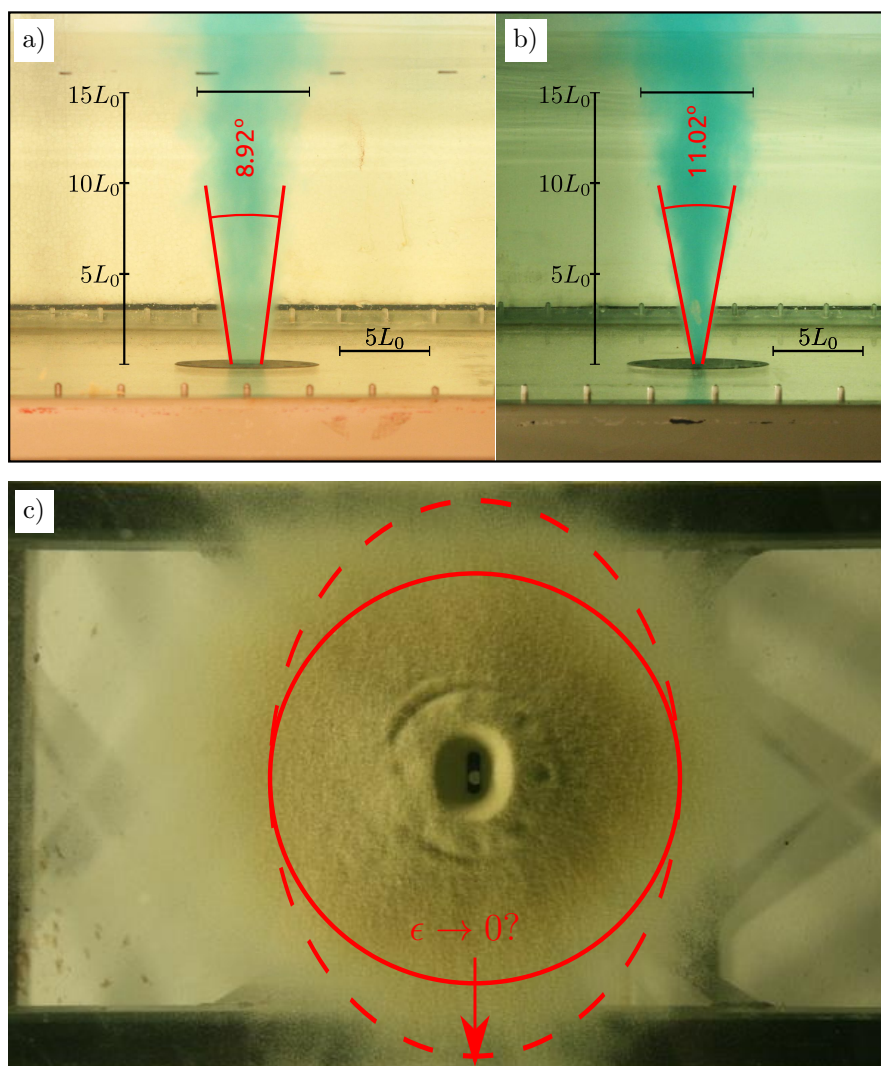


Figure 5: Experimental jet formed by a linear vent (expt. 23, $\epsilon = 0.41$) looking a) perpendicular and b) parallel to the long axis of the vent, the latter having a larger jet angle (given in degrees on both images). Scale bars, given in terms of L_0 , are shown in both images and the horizontal black bars at $z = 15L_0$ are of equal length. c) Example of a deposit formed by a linear vent. We highlight the approximately circular shape of the deposit (solid line). A smaller ϵ will give more elliptical deposits (dashed lines).

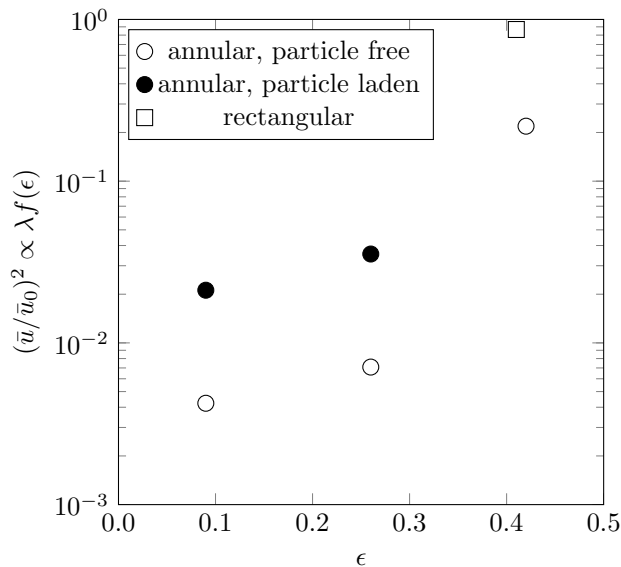


Figure 6: Prediction of KE in the jet relative to that present at the source as a function of ϵ . The functions, $f(\epsilon)$ depend on the geometry and ϵ of the vent and are given by (5)–(6).

265 5. Discussion and volcanological context

266 5.1. The distinct contributions of vent geometry and inertial particles to jet dynamics

267 Our results show that the entrainment coefficient, α_e , is affected by both the particle volume
 268 fraction, ϕ , and the gap size, ϵ . Entrainment is affected by gap size in two competing ways: first,
 269 small gaps generate an initial maximum eddy size that is small in comparison to the jet diameter, for
 270 example d_0 for a jet from an annular vent. Small eddies carry less angular momentum and consequently
 271 penetrate the ambient fluid to a relatively lesser extent leading, in turn, to reduced entrainment. As
 272 the largest eddies in a jet govern entrainment and their size is always constrained by the initial gap
 273 size, small gaps act to decrease α_e . This is particularly critical for high aspect ratio (i.e. elongated)
 274 vents. A second influence of the gap size on entrainment is through the shear strain rate at the source
 275 $\dot{\gamma} = u_0/l$, which is dimensionally the inverse of the eddy turnover time or the eddy rotation frequency.
 276 For narrow gaps, l is small. Thus, for a given average flow velocity, u_0 , shear strain rates and eddy
 277 rotation rates are high, which enhance entrainment.

278 Our results also suggest that the relative balance of the competing effects of gap size on the angular
 279 momentum flux carried by eddies and on the eddy turnover time vary with vent geometry. For jets
 280 from annular vents, a small gap relative to the overall vent diameter (small ϵ) have small eddies and
 281 a reduced α_e in turn. For linear vents, by contrast, the eddy size and jet width scale with each

282 other. Consequently the effects of vent width on the shear strain rate exert the strongest control on
 283 entrainment and ,accordingly, α_e increases with ϵ (figures 4 and 6). For example, in our experiments
 284 where the width of the linear vent was many times smaller than its length, the shear strain rate and
 285 α_e were larger in the direction perpendicular to the long axis (i.e. $l = l_w$), hence the larger jet spreading
 286 angles seen in figure 5.

287 We observe that geometric anisotropy in entrainment into jets imparted near the source of linear
 288 vents does not persist very high up the jet: the turbulent spreading of internal velocity gradients
 289 causes the jet to become axisymmetric by the time it rises $\approx 15L_0$ (figure 5) consistent with Glaze
 290 et al. (2011). This mixing property of the flow can explain the approximately circular deposits for
 291 $\epsilon = 0.41$ (figure 5c). However, the vertical extent over which this anisotropy in entrainment will persist
 292 is expected to increase as ϵ becomes small (and hence the magnitude of anisotropy becomes large).
 293 Thus, we expect deposits to be increasingly elliptical in shape as $\epsilon \rightarrow 0$.

294 Because, compared to jets from circular vents, jets from linear vents have a large perimeter com-
 295 pared to their cross-sectional area Glaze et al. (2011) argued that jets from linear vents entrain a
 296 greater volume of fluid for a given mean plume speed. However, our experiments suggest that for
 297 similar conditions of ϕ_0 , Ri_0 and approximately equal L_0 to the experiments of JJ14 (see curves for
 298 $\epsilon = 1$ in Fig. 4a), α_e is lower for linear vents. Furthermore, recent work on purely linear jets and
 299 plumes (i.e. $\epsilon \rightarrow 0$) has shown, assuming Gaussian profiles for velocity and buoyancy, that (Paillat and
 300 Kaminski, 2014a,b)

$$\alpha_{e,\text{linear}} = \sqrt{\frac{1 + \zeta^2}{2}} \text{Ri} \left(1 - \left(\frac{2}{3}(1 + \zeta^2) \right)^{-1/2} \right) + \frac{\sqrt{6}I_4}{2}, \quad (10)$$

$$I_4 = \int_{-\infty}^{\infty} \frac{\partial f(x^*, z)}{\partial x^*} j(x^*, z) dx^*, \quad (11)$$

301 where ζ is the ratio of the widths of the buoyancy and velocity profiles, I_4 is a dimensionless integral
 302 shape function involving the dimensionless velocity profile, $f(x^*, z)$, and turbulent shear stress profile,
 303 $j(x^*, z)$. A similar expression has been derived for round jets (Kaminski et al., 2005) where

$$\alpha_{e,\text{round}} = \text{Ri} \left(1 - \left(\frac{2}{3}(1 + \zeta^2) \right)^{-1} \right) + \frac{C}{2} \quad (12)$$

305 where C is a combination of shape factors (similar to I_4) whose value has been shown to be about

0.135 (Kaminski et al., 2005; Carazzo and Jellinek, 2012). Assuming that $\sqrt{6}I_4 = C$, comparing (10) and (12) shows that $\alpha_{e,\text{linear}} \leq \alpha_{e,\text{round}}$ for equal Ri independent of ζ . Hence we conclude that linear vents have a lower entrainment efficiency than circular vents. When $\phi \approx 0$, our results for a linear vent with $\epsilon = 0.41$ ($\alpha_{e,\text{linear}} \approx 0.075$) and an annular vent with $\epsilon = 0.42$ ($\alpha_{e,\text{round}} \approx 0.125$) agree with these calculations.

The presence of particles resulted in α_e increasing by 25–35% for all vent geometries we tested. An increase of α_e with ϕ was also observed by JJ14 for $\epsilon = 1$ vents with of a large diameter (see also figure 4a) giving $\alpha_e = 0.16$ compared to $\alpha_e = 0.15$ for particle-free jets. JJ14 deduced that the increased α_e is related to the additional angular momentum imparted by particles bound to eddies, which cause them to overshoot more deeply into, deform and engulf the ambient fluid. Additionally, the vent exit geometry (straight/flared, narrow/broad) focuses the particle momentum flux, causing eddy stretching: when the vent is narrow and straight, the particle flux acts to vertically stretch eddies thus reducing their penetration into the ambient fluid. Adding particles to jets from $\epsilon = 1$ vents with narrow diameter therefore decreased α_e from 0.15 to 0.09 despite the increased angular momentum from the particles. Decreasing ϵ leads to small eddies so we interpret the increased α_e in the relatively narrow $\epsilon = 0.09$ vents (where the gap size was approximately equal to the narrow vent diameter of the experiments reported in JJ14) as the gain in angular momentum due to presence of particles being of lesser effect than the vertical stretching of eddies.

The work required to overturn and mix the density interface between jet and ambient fluid is extracted from the KE of the jet (Linden, 1973). Our results show that more KE is expended to do the work of overturning and mixing when ϵ is small (figure 6), due to the lack of penetration of small eddies into the ambient fluid. Hence small gap size produces eddies that are small in comparison to the overall jet diameter which thus require more KE to overturn, mix and entrain fluid into the jet.

5.2. Collapse of jets during caldera-forming eruptions

Our results can be applied to identify and understand the conditions in which catastrophic caldera-forming eruptions from spatially continuous or discontinuous ring fractures are more likely to lead to jet instability, which causes collapse and the production of pyroclastic flows. The potential for a jet of given source conditions to collapse can be determined from the conservation equations (7). We numerically integrated this system of equations using a 4th-order Runge-Kutta solver with suitable source conditions for q_0 , m_0 and p_0 (figure 7). We consider particle-laden jets that are negatively buoyant at the source and that will collapse if they do not go through a buoyancy reversal. Hence

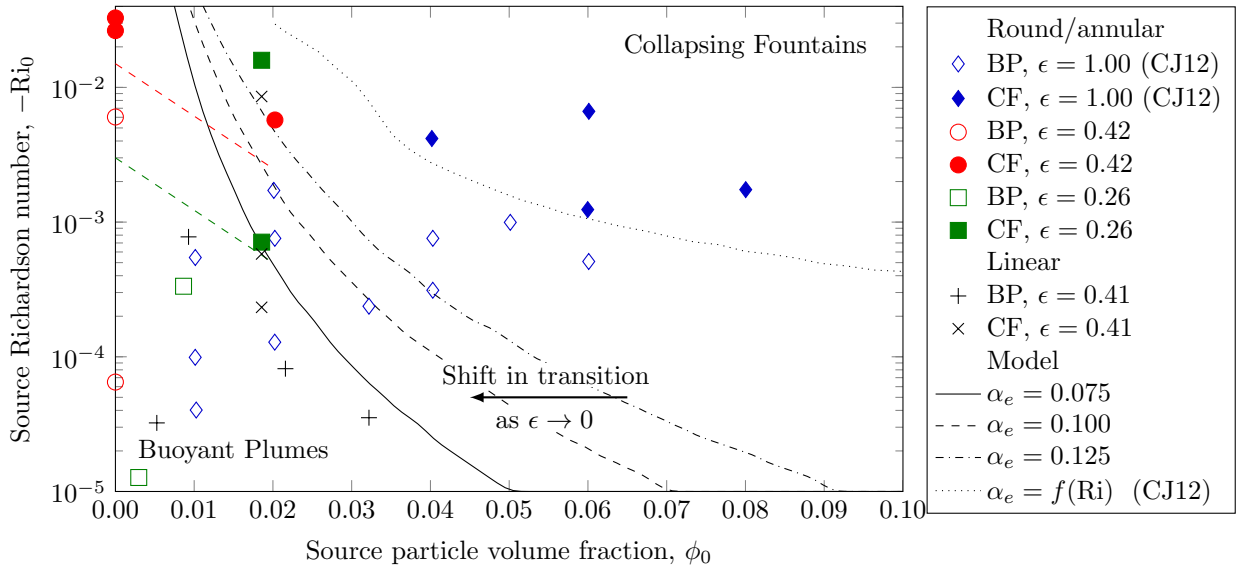


Figure 7: Regime diagram describing the theoretical transition between (stable) buoyant plumes and (unstable) collapsing fountains, given by the collapse model (7), as a function of ϕ at the source, ϕ_0 , and the source Ri , $-Ri_0$. The data points are the experiments from this study (cf. Table 1) and from Carazzo and Jellinek (2012) (CJ12) for a cylindrical vent (i.e. $\epsilon = 1$). The various lines give the theoretical transition from buoyant plumes to collapsing fountains using a top-hat model with different (constant) values of α_e as suggested from our experiments, and the variable entrainment model of CJ12. The arrow shows how they shift to the left as ϵ decreases. Coloured dashed lines show the approximate transitions shown by the data. In the legend text, BP = buoyant plume, CF = collapsing fountain.

337 if, for given initial conditions, g' remains negative at all altitudes then we determine that the jet will
 338 collapse.

339 Figure 7 shows a Ri_0 - ϕ_0 regime diagram for the formation of buoyant plumes/collapsing fountain
 340 from circular, annular and linear vents. We include our experiments that formed a buoyant plume
 341 (BP) or a collapsing fountain (CF) (table 1) as well as those reported in Carazzo and Jellinek (2012)
 342 which are for a round jet with $\epsilon = 1$. We calculate the theoretical transition from buoyant plumes
 343 to collapsing fountains for the present model as per Carazzo and Jellinek (2012) and show these as
 344 curves, though we use a constant values of α_e as determined from our experimental data (table 2). We
 345 also give the theoretical transition using a variable entrainment coefficient as was reported in Carazzo
 346 and Jellinek (2012). It is immediately apparent from the experimental data that collapse is more likely
 347 when ϕ_0 and/or Ri_0 are large but our experiments also indicate that collapses occur in annular and
 348 linear vents at lower values of ϕ_0 and Ri_0 than in circular vents. The theoretical transition is strongly
 349 dependent on the value of α_e , and the transition curves shift towards lower ϕ_0 and Ri_0 as α_e decreases,
 350 a trend which is also seen in the experimental data as ϵ decreases (equivalent in itself to decreasing α_e).
 351 This finding supports our observation that α_e decreases with decreasing ϵ for annular vents (figure 4a).
 352 The theoretical transitions come close to capturing the actual transition when the particle fraction

353 is greater than about 0.02, but perform more poorly when the particle fraction approaches zero. As
354 table 2 shows, α_e is lower for particle-free flows so that we expect a transition from larger α_e at large
355 ϕ_0 to lower α_e at low ϕ_0 . Hence theoretical models using a constant entrainment coefficient are poorly
356 suited to capturing the rise and spread of particle-laden jets, particularly from non-round vents. A
357 variable entrainment model (e.g. Carazzo and Jellinek, 2012, shown as dotted curve in figure 7) may
358 be more successful but there is currently no data with which the integral shape factors in (10) and
359 (12) can be constrained when jets contain particles or are produced from non-round vents.

360 In this context, we highlight that calderas have an overall diameter on the order of several kilometres
361 or tens of kilometres for a gap length (i.e. the ring faults) on the order of a hundred metres (Lipman,
362 1984) so that $\epsilon_{\text{caldera}}$ is of the order of 0.1 or less. The shift in transition curves as ϵ decreases shows
363 that collapse occurs for lower ϕ_0 and Ri. Hence we conclude that, for equal source conditions, volcanic
364 jets produced by annular ring fractures during caldera forming eruptions are more prone to collapse
365 and the emplacement of very-large scale ignimbrite deposits than jets from circular vents.

366 Our experiments involved symmetric annular vents. In nature, however, during subsidence of
367 piston-style calderas (e.g. Lipman, 1997), feedback between the sinking block and magma has been
368 shown to cause the block to tilt and shift laterally leading to azimuthal variation in the gap width
369 (Folch et al., 2001; Kennedy and Stix, 2007; Kennedy et al., 2008). Assuming variation in gap width of
370 the order of what we considered in experiments on linear vents that showed anisotropic entrainment, it
371 is possible that natural caldera eruptions may involve anisotropic entrainment because of the variation
372 in gap size during uneven sinking. Consequently, column collapse would occur soonest and even
373 preferentially where the vent is narrowest (hence having the locally lowest α_e), which may show up
374 in the deposit stratigraphy. We note also that during a piston-type caldera collapse, the width of an
375 annular vent may vary over time if collapse of the central piston is driven by steeply inclined reverse
376 faults, which opens the gap, while marginal blocks slide along associated normal faults, which closes
377 the gap (Roche et al., 2000). Such a pattern would lead to complex eruptive feedback effects in the
378 eruptive dynamics, leading to alternating phases of low or high entrainment rates and hence possible
379 successive buoyant jet phases and collapse events.

380 Jets from linear vents collapse at lower Ri₀ and ϕ_0 than for round or annular jets with equivalent
381 conditions (cf. data points for $\epsilon = 0.42$, annular vent and $\epsilon = 0.41$, linear vent in Fig. 7). This reflects
382 the comparatively low values of α_e estimated from the jet angle data. Very large MER eruptions from
383 linear vents have relatively large width compared to their length (Costa et al., 2011), so are likely to

384 have ϵ similar to our experiments and so will also have similar, low α_e . Large MER jets from linear
385 vents are therefore prone to collapse as, not only are they very dense as ϕ is large for large MER (see
386 table A.1 of the supplementary material), but they also have relatively small entrainment coefficients
387 and are hence less stable. This supports field observations of large volumes of ignimbrite deposits
388 linked to linear vent areas (Korringa, 1973; Aguirre-Diaz and Labarthe-Hernandez, 2003).

389 *5.3. Super eruptions produce a greater proportion of pyroclastic flows*

390 As shown in figure 1, owing to the influence of ϵ on jet stability as discussed above, the relationship
391 between V_i/V_t and M is likely not to be straightforward, particularly when the caldera diameter
392 becomes large. To test this, we have selected 17 silicic eruptions which represent a range of M from
393 5.4–9.1 for which at least two components out of the outer-caldera ignimbrite, intra-caldera fill and
394 tephra fall volumes are known. As per Mason et al. (2004) we take V_t to be the sum of the tephra fall,
395 intra-caldera filling and outer caldera ignimbrites. Our collated data is shown in figure 1 and given in
396 table B.2 (supplementary material). The intra-caldera fill volume by ignimbrite is hard to constrain
397 as i) caldera floor depth of often hard to determine unless there is full-depth faulting and ii) intra-
398 caldera fill also contains caldera collapse material (syn- or post-eruptive, e.g. Lipman, 1984; Wilson,
399 2008) and hence is often poorly constrained in terms of the actual volume erupted. The volume of
400 ignimbrite produced during silicic eruptions as a proportion of the total volume correlates with the
401 eruption magnitude, as suggested by the arrows in figure 1. Furthermore, the data suggests that the
402 proportion of ignimbrite increases drastically (slope doubles) at around $M_{\text{crit}} \approx 7.5$. Calderas that
403 form in eruptions where $M < M_{\text{crit}}$ (e.g. Katmai 1912) have very much smaller overall dimensions and,
404 assuming that the gap size is of the same order of magnitude than for large calderas, these correspond
405 to large ϵ in our experiments. The largest eruptions therefore have $\epsilon \ll 1$, resulting in decreased
406 entrainment and increased likelihood of PF formation. In determining the trends in figure 1, we have
407 neglected the data for Pinatubo, Krakatau, and Minoan eruptions and the Ito Tuff (dashed ellipse).
408 This was done for three reasons. First, strong winds carried much of the ash from the 1991 Pinatubo
409 eruption away to the southwest where it deposited in the South China Sea (Paladio-Melosantos et al.,
410 1996) making it nearly impossible to accurately estimate the amount of ash fall produced during
411 the eruption leading to higher estimations of V_i/V_t . Second, the Minoan and Krakatau eruptions were
412 strongly affected by water, meaning that the eruption dynamics were altered in favour of PF formation
413 as heat energy was used in the water-steam phase change and could thus no-longer drive the vertical
414 motion of the jet (Bond and Sparks, 1976; Self and Rampino, 1981). It is important here to note

415 that these two are also eruptions in near-coastal locations and as such much of the airborne ash may
416 have been lost to sea. The total eruption volumes would therefore be underestimated. Third, no
417 differentiation was made between ignimbrite and intra-caldera fill volumes for the Ito tuff (Aramaki,
418 1984).

419 **6. Conclusions**

420 Motivated by the enigmatic propensity of cataclysmic, caldera-forming eruptions to emplace very
421 large amounts of ignimbrite relative to the total erupted volume, we have undertaken a study into
422 the stability of particle-laden jets under conditions that are commonly found during the formation of
423 calderas. The fissures and ring dykes that form during caldera collapse, and transport the gas and
424 ash mixture to the surface, can be characterised as being either linear or annular vents. Furthermore,
425 catastrophic caldera forming eruptions involve a significant proportion of inertial particles, that is
426 particles with a Stokes number of the order of unity, that are critically coupled to the flow. Hence
427 both these vent geometries and inertial particles are critical to the stability of eruption columns and
428 ultimately determine whether an eruption predominantly produces buoyant plumes or pyroclastic flows.

429 We reproduced the dynamics of jets formed in explosive caldera-forming eruptions using scaled
430 laboratory experiments where a particle-water mixture was injected into a tank of water. In particular,
431 we varied the shape and aspect ratio of the vents through which these jets were formed in order to
432 reproduce a range of vent types seen in nature. Our results were combined with a one-dimensional
433 entrainment model to show that the presence of inertial particles and the aspect ratio of the vent
434 play an important role in determining the dynamics of volcanic jets and the related entrainment of the
435 ambient fluid or the collapse of the particle laden-mixture. Using this model, we measured entrainment
436 through an entrainment coefficient along with another parameter that compared the amount of work
437 required to overturn and mix the density interface forming the edge of the jet to the amount of kinetic
438 energy available to do this mixing. More specifically, our experimental results and analysis favour
439 three specific conclusions:

- 440 i) The kinetic energy (KE) extracted from turbulent jets to overturn the density interface compared
441 to the amount available at the source is large when the vent aspect ratio is small. The ratio of
442 KE extracted to KE available decreases as the aspect ratio increases.
- 443 ii) The addition of inertial particles to jets produced by straight-sided annular and linear vents

444 increased the entrainment coefficient because of the additional angular momentum transported by
445 turbulent particle-laden eddies.

446 iii) The entrainment coefficient decreases when the aspect ratio of the vent decreases because eddies
447 produced in jets from these vents are small compared to the diameter of the jet and therefore they
448 penetrate less far into the ambient fluid and hence entrain less fluid.

449 Reduced entrainment stems from mechanical effects imparted as the jet exits low aspect ratio
450 vents and these jets are unable to undergo a buoyancy reversal. When extended to volcanic jets, these
451 findings support the conclusion that jets from caldera-forming eruptions are more likely to collapse and
452 so produce pyroclastic flows. Therefore we should indeed expect to find that, by volume, ignimbrite
453 forms a larger portion of the deposits from caldera-forming eruptions but that this relationship is not
454 a straightforward function of eruption magnitude and, particularly, caldera size.

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